MUNSON TWP.

Bass Lake Road Extension

Chardon - Munson Town-Line Road

97

DIETZGEN

ENGINEER'S

FIELD BOOK

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Bass Lake Road - No. 23
Sections - D & E
Pg - 1 - 9 (1958 17)
X Sect Pg 15 - (1956 21769)

Thwing

Chardon - Munson Twp. Line Road
No. 27 - Sections A B C
Pg - 26 - 78

1952 references for pg 14 -

MUNSON SCHOOL BD 1954 Pg 10
" " " 1957 Pg. 14

42.50ch.
.66

25.5.0
25.5.0
2505.00

Road Record - Book 8 - Page 488

June 6 - 1831 Statute Width 60'

"Survey of a Road beginning in center of the State road leading from Chardon to Ravenna at the angle in said road South of the Beaver dam in Munson, thence running S. 28 3/4 W 42 chains 50 links.

Thence S. 30° W. 76 chains,
thence S. 13 1/2° W 28 chains 75 links,
thence S 1 1/2° E. 39 chains 75 links.
thence S. 2° 10' E. 30 chains 75 links to the northwest corner of lot No. 10, tract No. 3 in said Munson,
thence S. 1 1/2° E one mile 61 chains 33 links to the South line of Munson Township.
Surveyed April 27th 1831,
by George E. White, Surveyor.

1 mi. 80.00ch.
61.33
141.33
66.
84798
84798
9327.78 ft

39+70.8 Δ = 0°17' Right, Iron Pin in Center of Bridge, Both ways

18+50 Iron Pipe, Δ = 0°10' Left,

16+86 8" Tile, Extend W. End,

11+15 2 3' Long C.I. Pipe // Build New 15" square across road, Drain into field,

8+00 Iron Pipe Δ = 0°00'

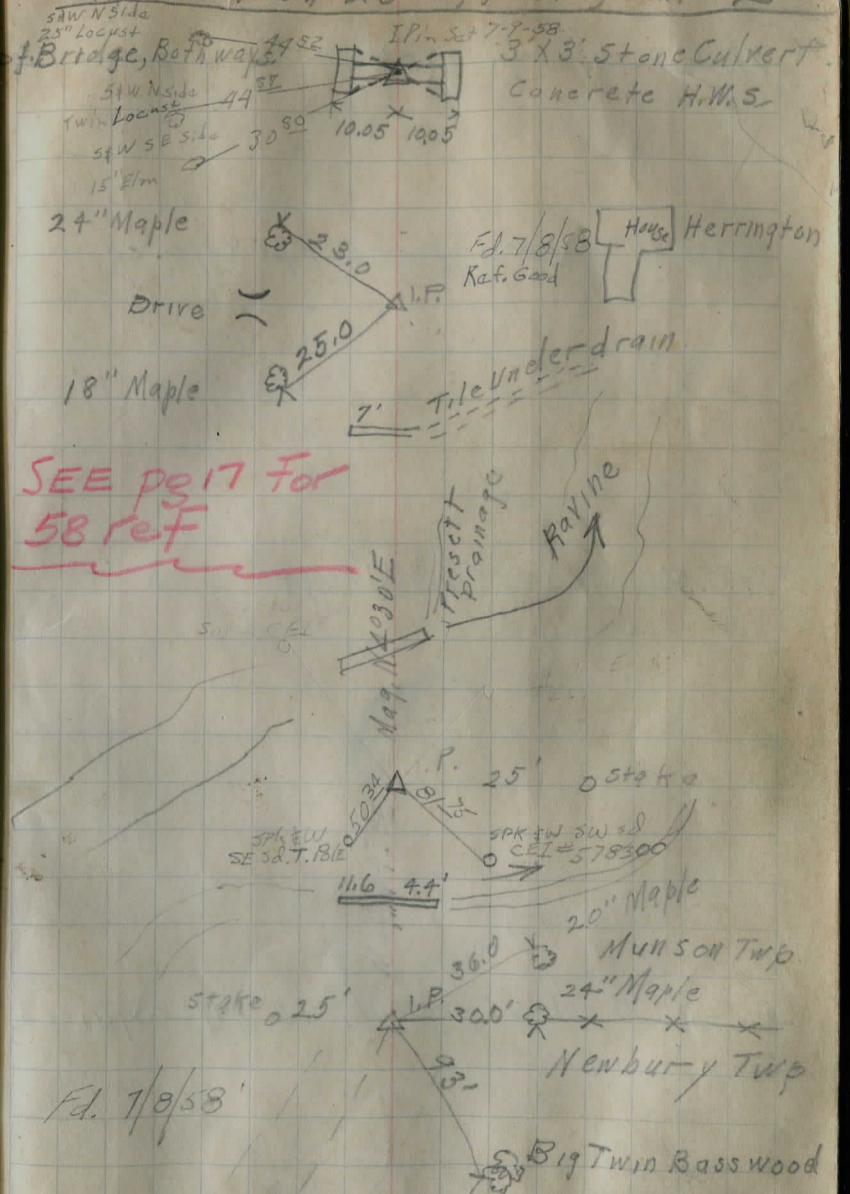
3+00 8" C.I. Pipe

0+00 Iron Pipe

BASS LAKE

CH # 23 Sec E of F

Stakes set on 25' offset from ℄ 2

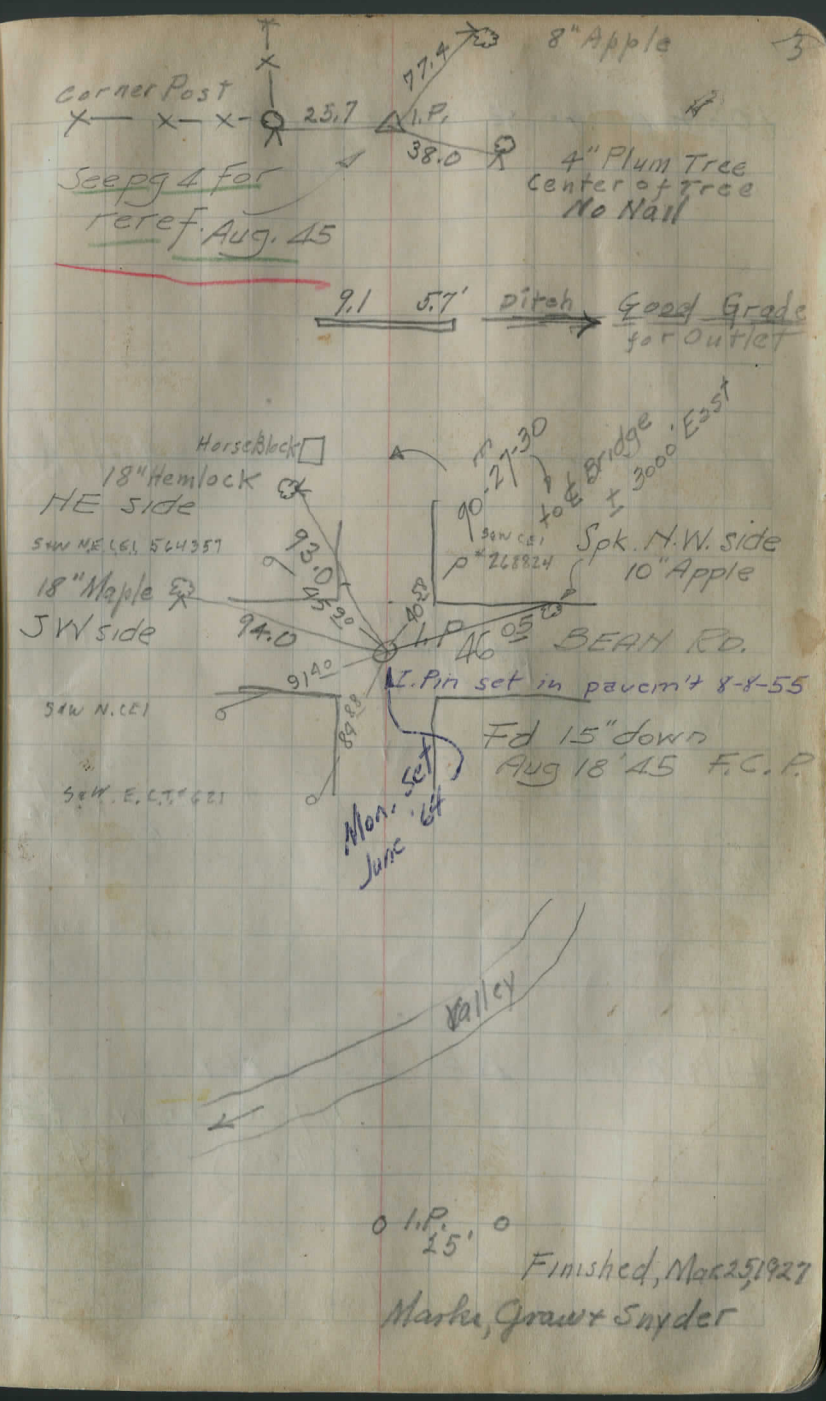


79+34.0 Iron Pipe Δ = 0°00'

68+19 12" Corr. pipe, broken — 12" Pipe Required

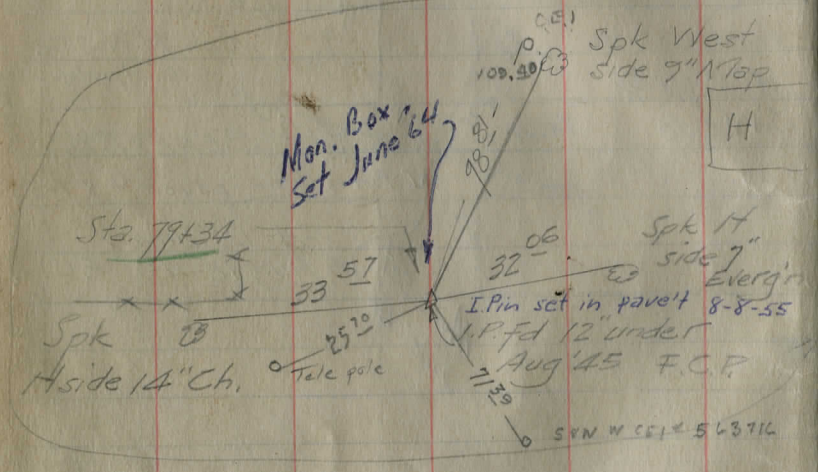
57+77.5 Δ = 00 25½' Left

56+00 No culvert present, — 12" Pipe required.



106+08.4, ℄ Mayfield Road

105+78.0, South Side Line of Mayfield Rd.



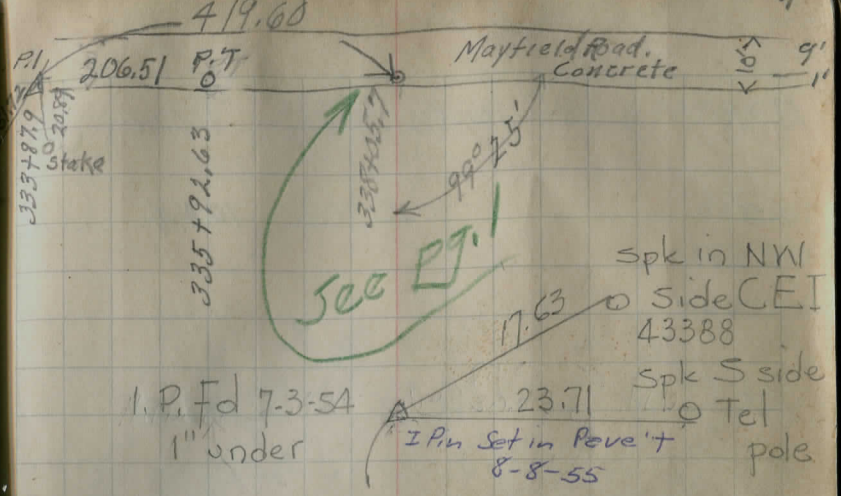
94+15.0 Δ = 0°31' Left

179-30 } on west
359-00 } 7-3-54

88+00 Δ = 0°00'

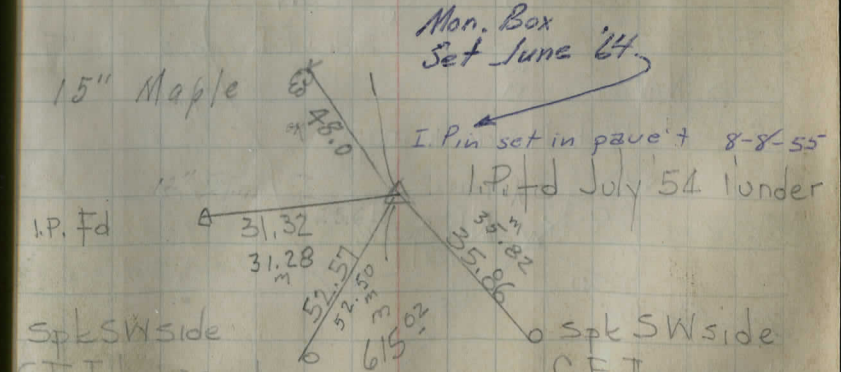
4

419.60'



1162.96

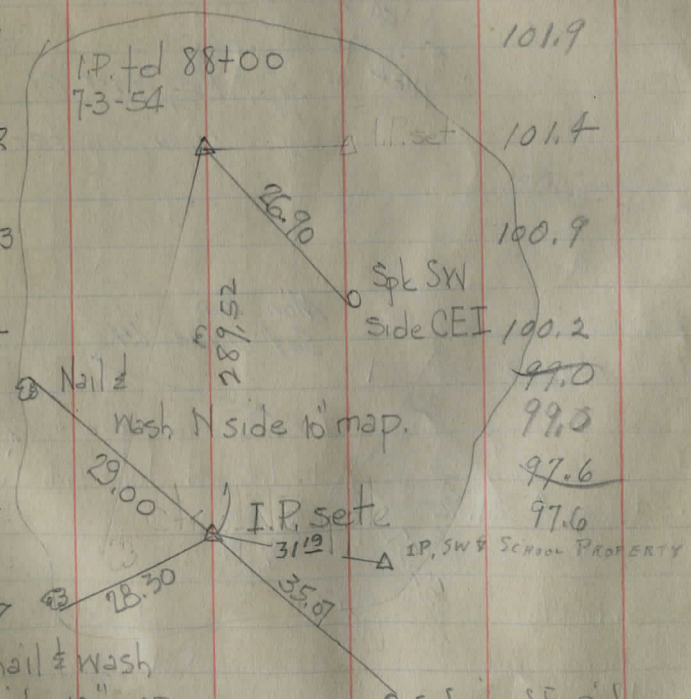
April 4, 1927, Cloudy, 40°
Marks, Grau, Snyder.



Mar. 29, 1927. Marks, Grau, Snyder
Fair.

Assumed El., N.W. cor., W.H.W. Culv. 39+70.8

B.M.	6.50	106.50	100.00
28			104.4
28+30			
28+60			
29			103.3
30			102.6
31			101.9
32			101.4
33			100.9
34			100.2
35			~~99.0~~ 99.0
36			~~97.6~~ 97.6
37			



104.4
2.1
0

66. Ditch
60 Ditch.
25 Ditch.

103.5 102.6 102.2 103.0 103.3 102.7 99.7 99.2 102.8 103.9 103.6
3.0 3.9 4.3 3.5 3.2 3.8 6.8 7.3 3.7 3.6 2.9
20 14 6 5 0 14 17 20 25 35 40
Fence

102.6 101.1 102.3 101.8 102.4 102.6 101.8 99.4 99.1 102.6 103.4
3.9 5.4 4.2 4.7 4.1 3.9 4.7 7.1 7.4 3.9 3.1
21 14 8 7 5 0 15 19 23 27 40
Fence

101.8 100.9 101.9 101.2 101.8 101.9 101.8 99.7 98.0 98.5 102.3 101.6 101.9
4.7 5.6 4.6 5.3 4.7 4.6 4.7 6.8 8.5 8.0 4.2 4.9 4.6
21 14 9 7 6 0 14 19 21 24 30 35 40
F

101.6 100.7 100.1 101.1 100.3 101.0 101.4 100.7 98.7 97.2 98.3 101.8 101.2 101.9
4.9 5.8 6.4 5.4 6.2 5.5 5.1 5.8 7.8 9.3 8.2 4.7 5.3 4.6
20 15 12 9 8 6 0 11 15 17 20 27 31 38
F

101.5 100.8 99.5 99.7 100.4 100.9 100.3 98.4 97.1 101.4 101.3
5.0 5.7 7.0 6.8 6.1 3.6 6.2 8.1 9.4 5.1 5.2
21 15 14 10 7 0 12 16 17-20 26 40
F

100.6 98.5 99.1 98.8 99.5 100.2 99.7 100.4 97.6 96.1 96.9 97.9 100.1 100.5
5.9 8.0 7.5 7.7 7.0 6.3 6.8 6.1 8.9 10.4 9.6 8.6 6.4 6.0
21 16-13 11 9 7 0 9 10 15 16-18 19 21 25 40
F

99.8 98.1 98.1 97.6 98.5 99.0
6.7 8.4 8.4 8.9 8.0 7.5
21 16 11 9 8 8
F

98.5 96.8 95.6 98.5 99.3 99.4
8.0 9.7 10.9 8.0 7.2 7.1
12 15 16-18 22 25 40

98.6 97.7 97.4 97.1 97.4 97.6
7.9 8.8 9.1 9.4 9.1 8.7
21 18 12 10 8 0
F

96.9 97.1 95.7 98.4 98.4
9.6 9.4 10.8 8.1 8.1
8 14 17-19 23 40

31.19

Sta.	H.I.	Az.	Dist.	Rod	El.
℄ 39+70.8 = 28+00	103.75	88°00 90°15'			
		90°	15.	9.1	94.7
		43°	34	10.2	93.6
		77°30'	178	10.2	93.6
		72°40'	210	10.0	93.8
		71°40'	215	9.9	93.9
		52°05'	410	12.4	91.4
		61°30'	550	13.6	90.2
B.M	3.70	103.70		100.00	
37				97.3	
38				96.7	
39+00				97.4	
39+70.8				98.5	
40+				98.4	
41+				99.4	
42				99.0	

Fence
Ditch
"
"
"
"
"
"

97.3 97.1 96.6 97.1 97.3 96.6 97.2 96.4 95.2 96.8 97.7 97.8 97.4
6.4 6.6 7.1 6.6 6.4 7.1 6.5 7.3 8.5 6.9 6.0 5.9 6.3
21 13 10 9 0 11 12 15 16 19 20 22 26 40

97.1 96.8 96.0 96.2 97.2 96.7
6.6 6.9 7.7 7.5 6.3 7.0
21 15 14 11 9 0
F

96.8 94.9 95.2 96.6 97.5 96.7 97.1
6.9 8.8 8.5 7.1 6.2 7.0 6.6
13 16 19 20 22 27 40

96.7 96.0 97.1 97.4
7.0 7.7 6.6 6.3
22 15 - 11 10 0

97.0 95.0 96.6 97.1 96.7 96.5
6.7 8.7 7.1 6.6 7.0 7.2
12 16-19 20 22 25 40

97.3 96.3 95.2 94.6 97.5
6.4 7.4 8.5 9.6 6.2
28 18 15 10

100.0
3.7
10 - 8.5

98.5
5.2
8.5 - 0 - 8.5

99.9
3.8
8.5 - 10

97.4 94.7 94.5 95.2 96.3 97.0
6.3 9.0 9.2 8.5 7.4 6.7
10 15 19 21 24

96.4
7.3
33 - 40

98.9 98.0 97.6 97.9 98.2 98.4
4.8 5.7 6.1 5.8 5.5 5.3
30 25 17 16 15 11 0

98.4 96.7 97.8 96.8 96.4
5.3 7.0 5.9 6.9 7.3
8 9 10 25 28

100.8 100.2 99.2 99.0 99.3 99.4
3.9 3.5 4.5 4.7 4.4 4.3
25 14 10 9 8 0

99.1 98.7 97.4 98.5 99.2 F 99.6
4.6 5.0 6.3 5.2 4.5 4.1
18 11 14 15 25 27

99.7 99.4 98.4 99.0
4.0 4.3 5.3 4.7
25 17 9 0

98.7 97.5 98.7 99.1
5.0 6.2 5.0 4.6
10 13 15 27
F

	3	103.70	3.60	100.10
	3.60	103.70		
43				98.7
44				98.5
~~45~~				
45				99.0
46				99.7

99.7	98.9	98.3	97.6	98.3	98.7	
4.5	4.8	5.4	6.1	5.4	5.0	
25	18	10	9	6	0	
98.1	98.2	98.4	97.7	98.4	98.5	
5.6	5.5	5.3	6.0	5.3	5.2	
100	25	9	8	6	0	
95.1	96.6	97.4	98.5	99.0	98.1	99.0
8.6	7.1	6.3	5.2	4.7	5.6	4.7
200	83	82	13	10	8	6
↑ Ditch						0
	98.9	99.2	99.0	99.6	99.4	99.7
	4.8	4.5	4.7	4.1	4.3	4.0
	100	25	19	10	8	0

					98.1	97.6
					5.6	6.1
					9	11
96.3				98.5	97.7	97.3
7.4				5.2	6.1	6.4
100.				11	17	25
				99.0	98.0	97.6
				4.7	5.7	6.1
				12	18	25
99.2	99.5	99.7	98.9	98.5	97.3	
4.5	4.2	4.0	4.8	5.2	6.4	
7	8	11	20	25	100	

9-29-42
Pom.-Gun.

LEVELS

Note: Sta. 0 to : outlet end corr. I.P. at Warner's drive & stationing runs N½ & E½

	+	H.I.	−	E	
15			10.5	90.7	
14			9.9	91.3	
13+0			8.8	92.4	
11+0			7.1	94.1	
T.P.	3.90	101.16		97.26	11+0
5			10.4	95.4	
4			9.7	96.1	
F.L. drive pipe			7.4		
3+0			9.3	96.5	
6+0			10.0	95.8	
T.P.	6.86	105.81	4.38	98.95	6+0
T.P			6.07	97.26	11+0
9+0			9.3	94.0	
B.M.	3.33	103.33		100.00	

BASS LAKE ROAD

SEC'D pt.

Note: Road culvt = Sta 9+03

See Grades next pg.

(Assumed) N.W. & West hdwl

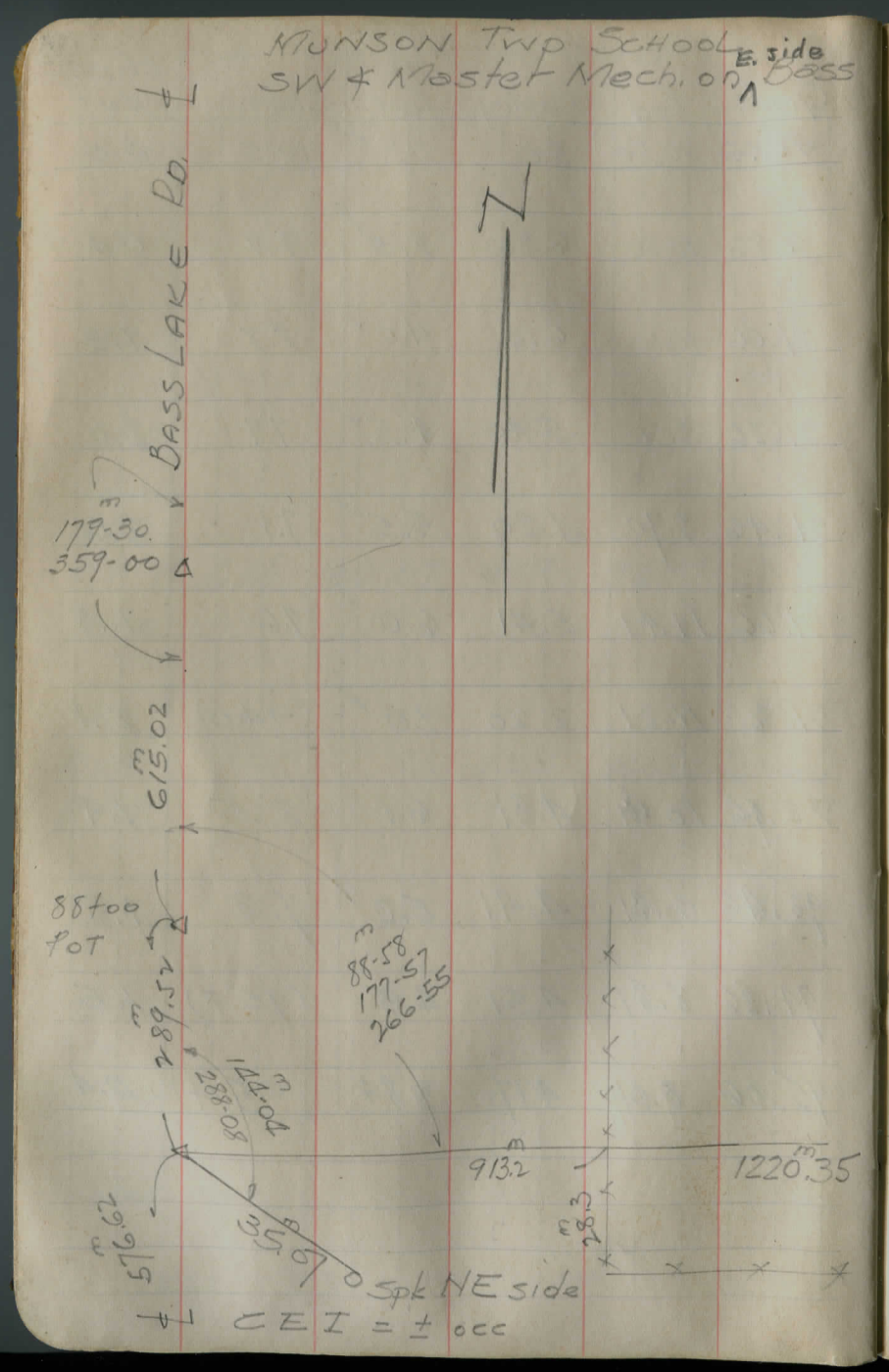
	+	H.I. 101.16	−	E
15+0				
14+0				
13+0				
12+0				
11+0				
T.P.	6.10	103.07	4.19	96.97
10+0				
9+0				
B.M.			3.05	100.02
8+0				
7+0				
6+0				
5+0				

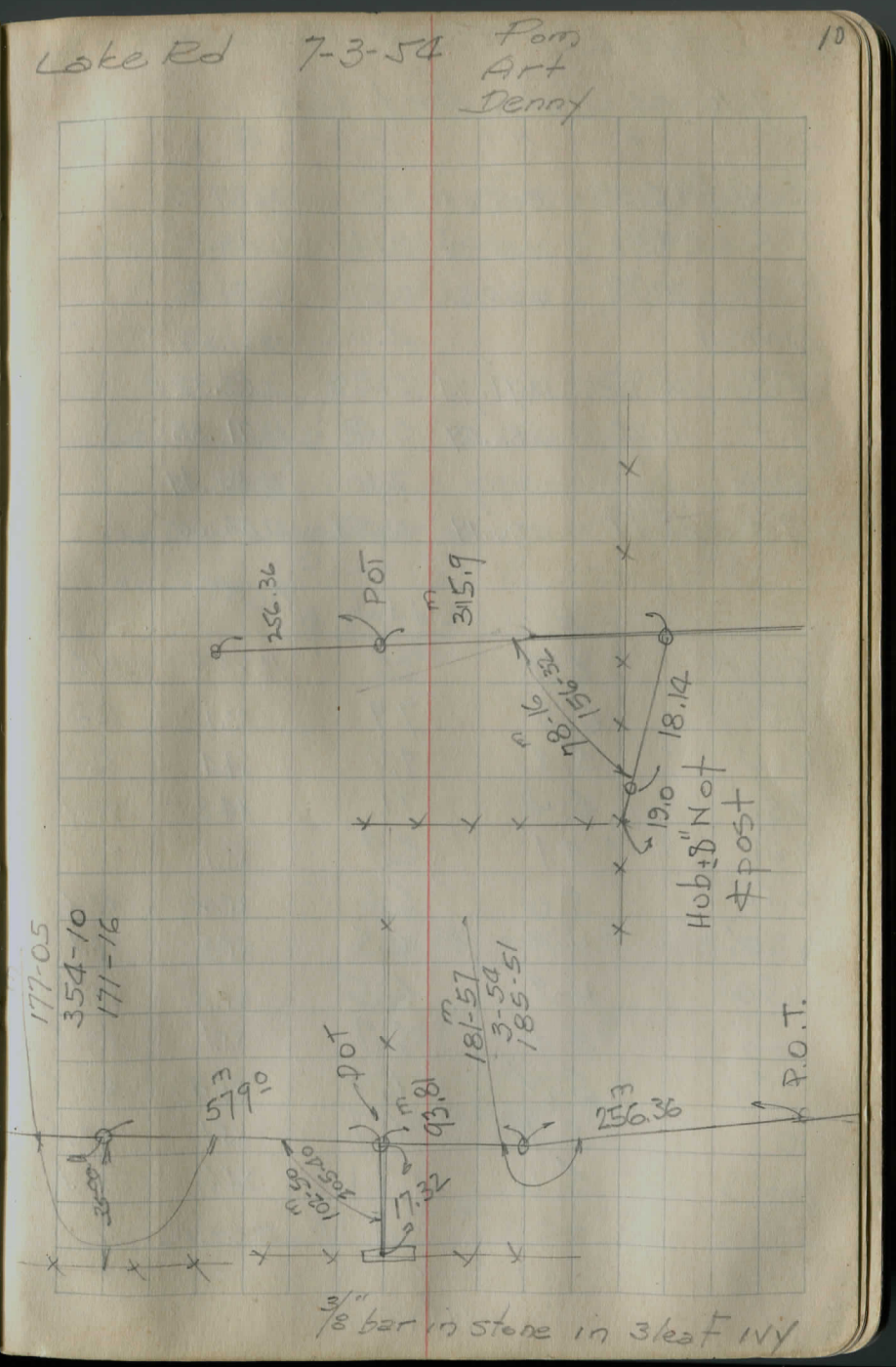
0.20% G.

0.80% G.

(100.00)

Grade	Rod	Reading	Top of Stk Cut	Chan.	Chan. cut
90.66	10.50	8.0	2.5	10.5	0.0
90.86	10.30	6.80	3.5	9.9	0.4
91.06	10.10	6.10	4.0	8.8	1.3
91.26	9.90	5.40	4.5	7.9	2.0
91.46	9.70	4.20	5.5	7.1	2.6
91.66	11.41	5.41	6.0	9.6	1.8
91.86	11.21	2.20	9.0	(94.0)	2.1
92.66	10.41	4.31	6.1	8.5	1.9
93.46	9.61	4.41	5.2	7.8	1.8
94.26	8.81	4.51	4.3	(95.8)	1.5
95.06	8.01	4.17	3.84	(95.4)	0.4


MUNSON Twp School
SW ✱ Master Mech. on
E. side
Bass
N
BASS LAKE RD.
179-30
359-00
615.02
88+00
POT
289.52
144.04
288.08
88-58
177-57
266-55
913.2
1220.35
28.3
29.62
35.0
Spk NE side
CEI = ± occ


Lake Rd 7-3-54 Fom
Art
Denny
10
256.36
POT
315.9
78-16
18.14
19.0
Hub ±8" Not
± post
177-05
354-10
171-16
579.10
POT
93.81
181-57
3-54
185-51
256.36
P.O.T.
17.32
3/8" bar in stone in 3 leaf ivy

LEVELS FOR MUNSON

7-10-54 John Art Pom

	+	HI	−	E	
BM Fd	6.33	1245.69		1239.36	
T.P.	9.52	1255.07	0.14	1245.55	
T.P.	10.76	1265.62	0.21	1254.86	
BM set			4.06	1261.56	
T.P.	8.42	1271.74	2.30	1263.32	
T.P	11.26	1282.59	0.41	1271.33	
BM			2.10	1280.49	
T.P	8.19	1290.19	0.59	1282.00	

Edith ↑ down

	℄			
500'N	6.9	8.6	1283.3	1281.6
450'	6.3	7.9	83.9	82.3
400'	5.8	7.4	84.4	82.8
350'	5.4	7.1	84.8	83.1
300'	5.1	6.9	85.1	83.3
250'	5.0	6.6	85.2	83.6
200'	4.9	6.5	85.3	83.7
150	4.9	6.5	85.3	83.7
100'	5.1	6.7	85.1	83.5
50	5.2	6.7	85.0	83.5
0	5.1	6.7	85.1	83.5
100'S	5.6	7.1	84.6	83.1
		4.77	1285.82	

SCHOOL PROPOSED

X in ledge rock E side V. Warner hse drive ± 38' N of ℄ #322 ± 5' SW of 24" Oak ± 7' SE of twin 18" So. map

Spk SE root 12" Map ± 100 W of Bass Lake Rd ± 35' N ℄ 322

SE ∠ bottom step cement block hse with 2 upstair dormer windows W side Bass Lak Rd ±1200' S of 322

℄

427 ≠

278 20.5 ≠ CEI s & telephone

127' ≠

0-25 20.3 ≠

℄

Spk NE side CEI ± 20' S of S P/L

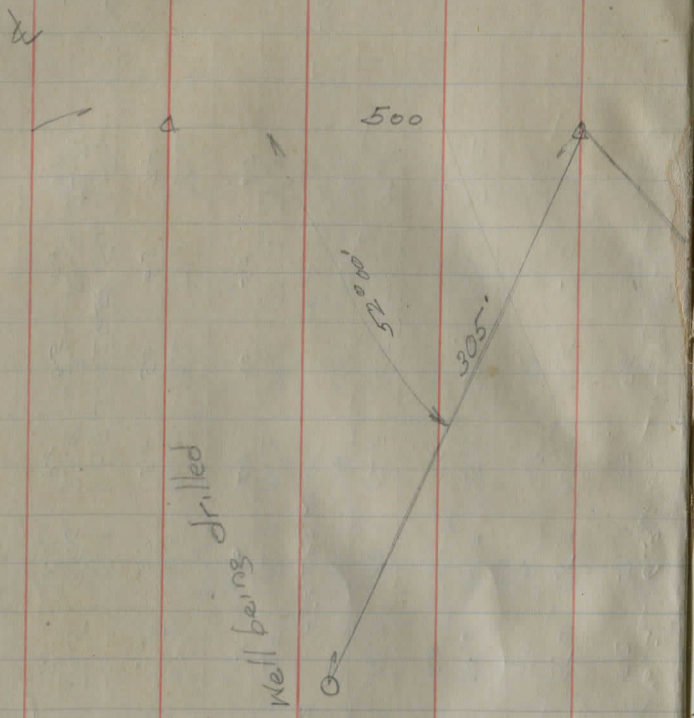
NIXON SCHOOL PROPOSED
Art John Rom 7-17-54

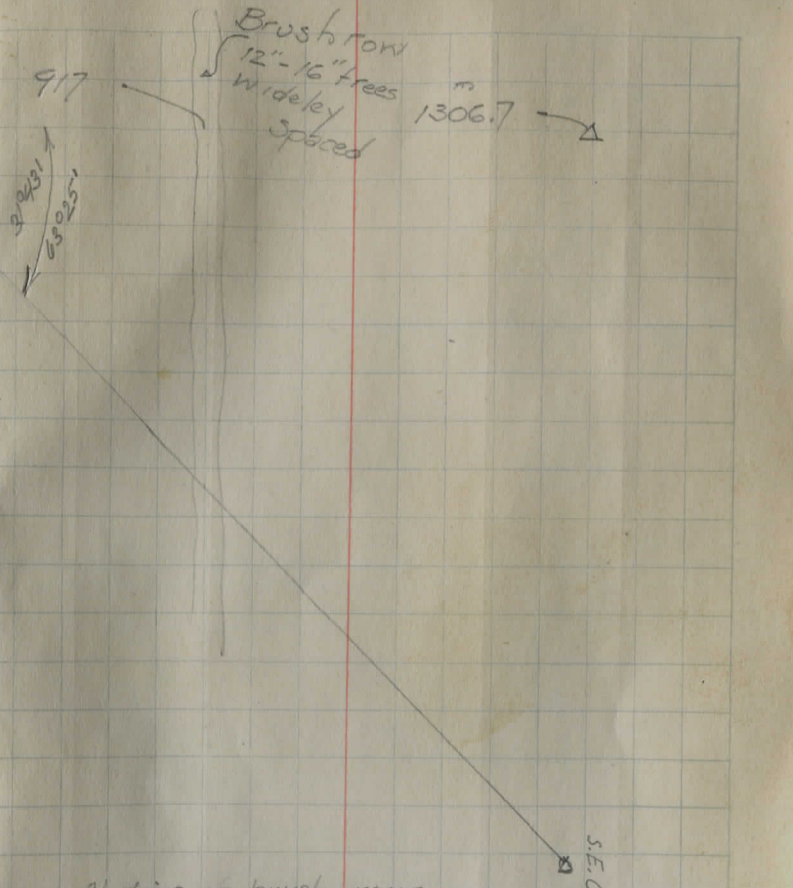
BM 5.95 1291.37

1285.42

	0	50	100	150	200	250	300	350	400	450	500	600
	← South P/L											
℄												
30	84.8 / 6.6		85.2 / 6.2		85.7 / 5.7		85.6 / 5.8		85.2 / 6.2		84.2 / 7.2	
100	84.2 / 7.2	84.6 / 6.8	85.1 / 6.3	85.6 / 5.8	86.1 / 5.3	86.2 / 5.2	86.4 / 5.0	86.3 / 5.1	85.9 / 5.5	85.1 / 6.3	84.2 / 7.2	
150	83.7 / 7.7	84.4 / 7.0	85.0 / 6.4	85.8 / 5.6	86.4 / 5.2	86.5 / 4.9	86.6 / 4.8	86.5 / 4.9	85.8 / 5.6	84.7 / 6.7	83.6 / 7.8	
200	82.8 / 8.6	83.4 / 8.0	84.6 / 6.8	85.5 / 5.9	86.2 / 5.2	86.7 / 4.7	86.5 / 4.9	86.2 / 5.2	85.1 / 6.3	83.9 / 7.5	82.7 / 8.7	
250	81.1 / 10.3	81.6 / 9.8	83.3 / 8.1	84.7 / 6.7	85.5 / 5.9	86.2 / 5.2	86.3 / 5.1	86.1 / 5.3	84.8 / 6.6	83.1 / 8.3	81.5 / 9.9	
300	78.4 / 13.0	79.8 / 11.6	82.0 / 9.4	83.6 / 7.8	84.8 ✓ / 6.6	85.4 / 6.0	85.3 / 6.1	84.9 / 6.5	83.5 / 7.9	82.0 / 9.4	80.3 / 11.1	
350	77.4 / 14.0	79.7 / 11.7	81.9 / 9.5	83.0 / 8.4	84.0 / 7.4	84.6 / 6.8	84.7 / 6.7	83.8 / 7.6	82.4 / 9.0	80.9 / 10.5	79.2 / 12.2	
400	75.5 / 15.9	78.9 / 12.5	81.2 / 10.2	82.4 / 9.0	83.4 / 8.0	83.7 / 7.7	83.4 / 8.0	82.3 / 9.1	80.7 / 10.7	79.3 / 12.1	77.9 / 13.5	
TP			-11.26	1280.11 ✓	3.+52		HI = 1283.63 ✓			Hub ± 80' N of 5 P/L ±450' back		
450	74.6 / 9.0	77.7 / 5.9	80.5 / 3.1	81.4 / 2.2	81.9 / 1.7	82.5 / 1.1	82.0 / 1.6	81.2 / 2.4	79.6 / 4.0	78.2 / 5.4	76.9 / 6.7	
500	73.9 / 9.7	77.2 / 6.4	79.5 / 4.1	80.6 / 3.0	81.0 / 2.6	81.2 / 2.4	80.9 / 2.7	80.0 / 3.6	78.6 / 5.0	77.3 / 6.3	76.2 / 7.4	
									7.09	B.M. 1276.54	500' L Pon N line	
600	70.3 / 13.3	72.7 / 10.9	74.2 / 9.4	75.6 / 8.0	76.4 / 7.2	76.5 / 7.1	75.6 / 8.0	73.8 / 9.8	73.1 / 10.5	73.2 / 10.4	72.7 / 10.9	
	TP	-	ELEV.	+		HI						
		11.47	1272.16 ✓	1.58		✓ 73.74						

continued next page





	+	H I	−	E
TP	1.58	1273.74 ✓	11.47	1272.16 ✓
			12.1	61.6
TP	0.85	1263.06 ✓	11.53	1262.21 ✓
			5.2	57.9
			6.5	56.6
			12.4	50.7
			12.7	50.4
			20.4	42.7
			15.5	47.6
			24.0	39.1

N. line, brush row

brush row, 197' from S. line, head end ravine running N.E.

S. end brush row

I.P. S.E. Cor

130' from S.E. Cor on E. line

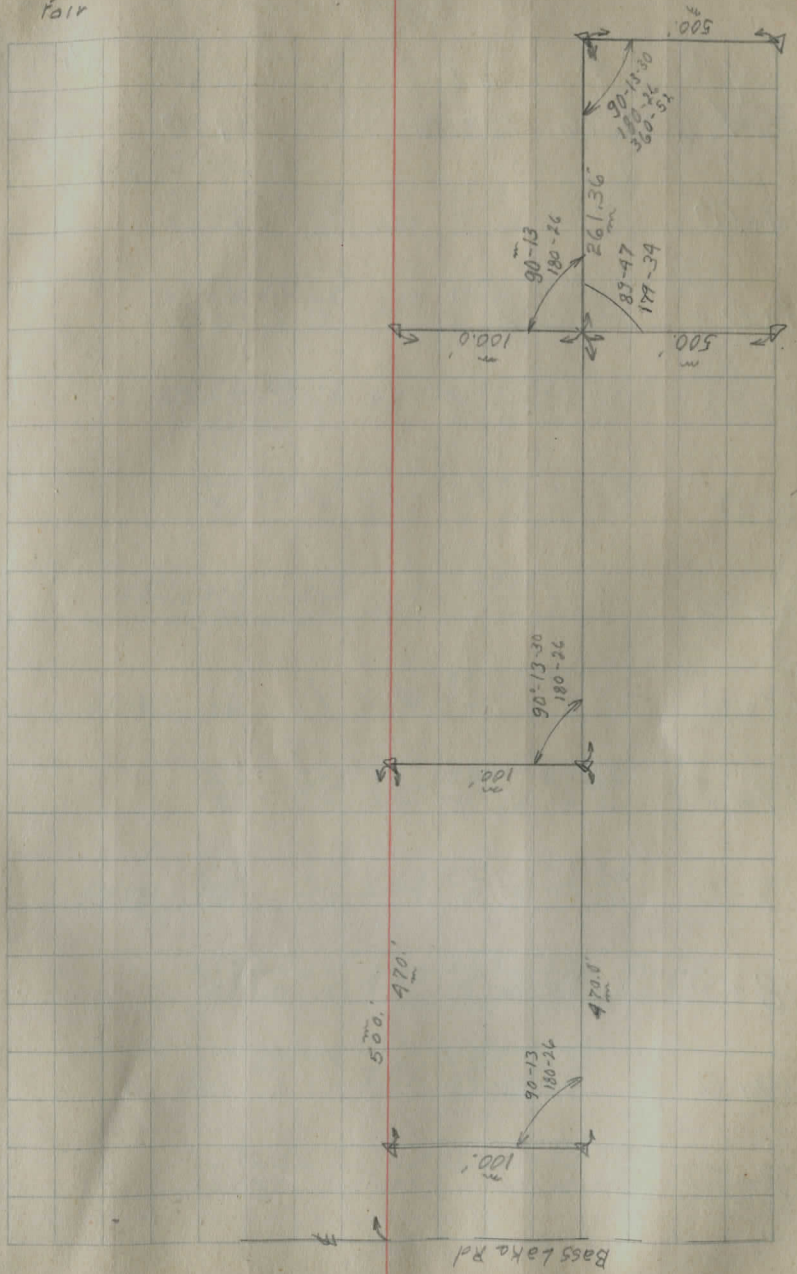
259' from S.E. Cor. on E. line

360' " " " " " "

I.P. N.E. Cor

3/16/57 Munson School

Fair



CROSS SECTIONING CH 23
STA 14+50 TO 22+50

PATTERSON
CANFIELD
ADAMS
YOUNG
4/8/56

	+	H.I.	−	ELEV.
B.M.	3.86	103.86		100
14+50				
15+0				
15+50				
16+0				
16+50				
17+0				
17+50				
18+0				
18+50				
19+0				
19+50				

(S)

HOR. SPK & W IN IP W 3d. CEI F 577799

STA ± 19+15

0.0/30 −1.0/23 3.10/14 0.95/10 ± 0.20 1.1/11 2.2/14 2.0/20 2.0/30

1.2/30 1.6/21 4.2/14 2.8/10 2.30 3.35/11 4.1/14 0.5/24 OUT/30

4.85/30 5.0/23 7.60/17 4.38/9 3.85 4.85/11 5.55/14 4.15/21 3.7/30

8.40/30 8.45/17 5.80/9 5.07 6.21/11 7.0/14 6.2/18 5.85/30

(E) DRVWY. 4.48/30 6.10/9 6.15 7.07/10 7.88/14 6.8/20 6.7/30 (W)

DRVWY. 11.0/30 7.8/9 6.98 7.47/9 8.33/13 7.28/18 OUT/30

8.26/30 7.40/10 6.65 7.44/10 7.7/14 6.9/19 6.85/30

DRVE. 5.30/30 6.16/11 5.44 6.24/10 6.64/13 3.5/19 4.4/30

3.26/30 2.2/20 4.83/9 4.80 4.6/9 3.0/24 2.98/30 DRVE.

3.55/30 4.25/16 7.85/10 7.50 8.45/13 5.97/18 5.37/30

8.13/30 8.41/28 12.7/9 11.65 12.1/11 12.55/14 9.75/21 9.70/30

(N)

	+	H.I.	−	ELEV
T.P	0.26	94.55	9.57	94.29
20+0	0.26			
20+50				
T.P	1.36	86.08	9.89	84.72
21+0				
21+50				
22+0				
22+50				
T.P.	11.84	97.87	0.05	86.03
T.P.	7.37	103.80	1.44	96.43
BM	3.78		3.78	100.02

S

E

W

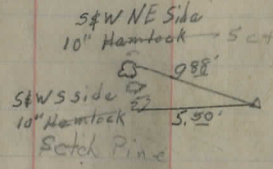
N

	3.62/30	4.76/20	7.10/12	6.06	6.69/10	7.9/14	5.94/22	5.60/30
	OUT/30	9.93/20	10.21/14	9.74/10	9.10	9.56/10	11.0/13	9.30/19	9.30/30
	3.4/30	3.4/24	3.76/15	3.25/10	2.66	3.22/10	4.1/13	3.4/30	
	4.36/30	4.4/21	5.3/17	4.0/8	3.78	4.4/9	5.6/12	4.75/18	5.3/30
E	DRVE 5.11/30			4.78/9	4.60	5.29/8	7.5/13	6.4/18	OUT/30
	5.51/30	6.9/14	5.87/10		5.40	6.36/11	8.0/14	7.31/17	7.1/30

July 9, 1968 Bass Lake Rd #23

H. Patterson
T. Adams
P. Young

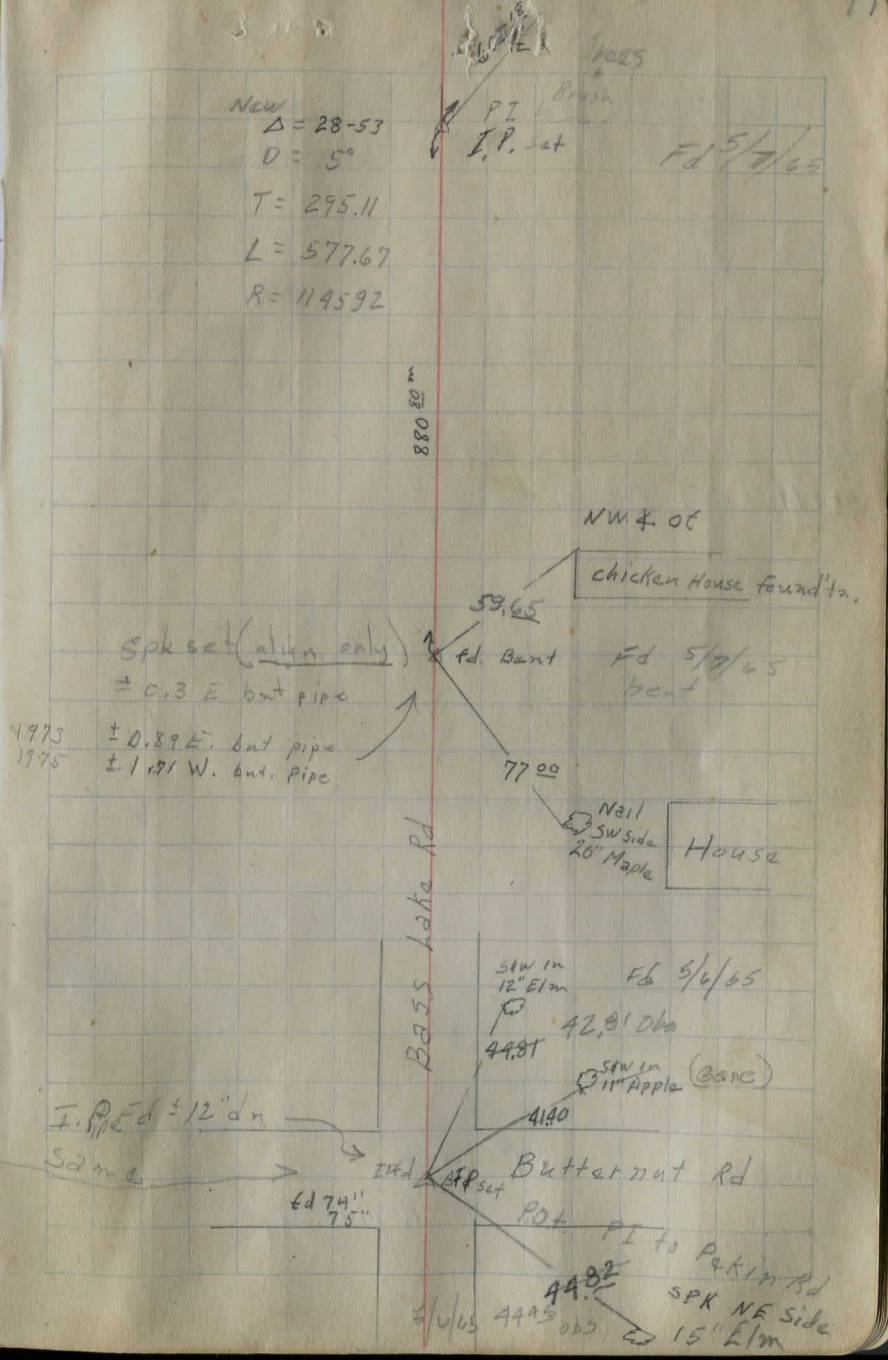
14+35.80



5+55.00 Iron Pipe fd.-58 Δ = 0°00'

0 to 0 Δ = 0°-00'

17



179.00
29-53
150.07

28+14.88
20+28.43
786.45

28+41.29 New
28+14.88 old Δ = 0°00'

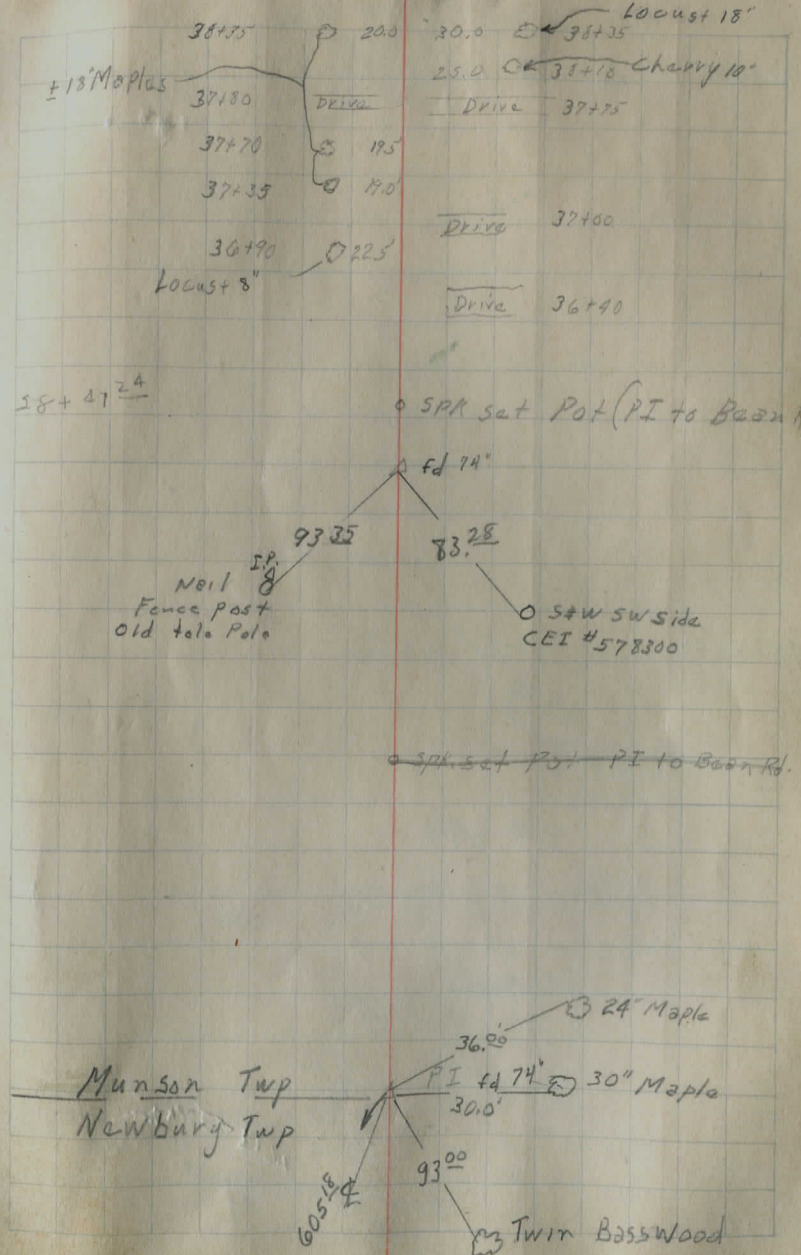
28+41.29
20 28.43
8 12.81

28+14.88
20+28.43
786.45

~~28+41.29~~

29-40-20
59-21

20+28.43 Δ = 29°-53'
D = 5° R = 1145.92
T = 302.94'
L = 592.33'



59+84.20 Δ = 0° 17' 30" Rt. I.P. Set

48+89.28

94+06 = end Pavement

20" Maple

47.88

90+84.03

26.14 SPK M.W. Side 20" Maple

38+65.09 SPK .50' W of I.P.

Drive 25.0' I.P. ℄ 74'

25.0'

18" Maple

IP ℄

5th W N side 25" Locust

3.03

44 52 SPK

4.05' SPK. Set P.O.T. PI to Bean

44 57

5th W N side Twin Locust

30.89

5th W SE side 15" Elm

N

12+0 13.5'

13+0 13.5'

14+0 14.5'

15+0 15.5'

14.5'

13.5'

12+0 12.5'

8+0 15.5'

9+0 17.0'

10+0 18.5'

11+0 16.0'

11+50 55.0

5th W SW side CEE #577794X

39.22

60.47

5th W SW side 16" Twin W. Cherry

Drive 42+0

41+50 17.5'

40+50

17.5'

17.5'

Brush

Brush

Maples 18"

39+30 19.5'

39+0 19.0' 20.0 39+0 30" Maple

38+62 Maple 22" 19.3 21.0 38+65 15" Maple

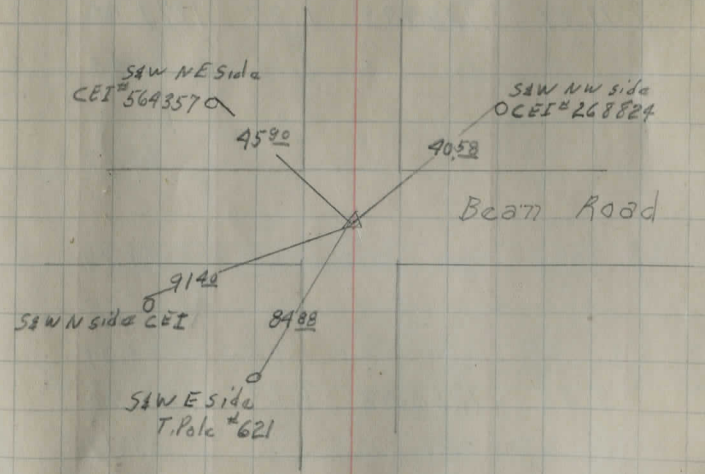
9.0' Conc Slab

Drive Drive 38+40

SPK Set POT PI to Bean Rd.

77+92.50

IP fd.
flush Pvt.



H. Patterson
D. Canfield
P. Young

Bass Lake Road

8-6-58 Cloudy 75°

	+	HI	−	Elev	
BM	2.71	1272.81		1270.10	
TP	9.08	1279.00	2.89	1269.92	See Pg. 59 This Book
T.P.	6.12	1280.73	4.39	1274.61	
BM #1	4.29	1280.63	4.39	1276.34	
TP	9.14	1278.82	4.95	1269.68	
TP	3.25	1274.70	7.37	1271.45	
B.M.				1270.05	
BM #1	4.39	1279.83		1275.44	✓
1+0				1274.93	
2+0				76.21	
TP	11.97	1289.93	1.87	1277.96	✓
3+0				78.43	
4+0				82.17	
5+0				83.79	
6+0				83.33	
T.P. 2	2.48	1285.38	7.03	1282.90	✓
7+0				81.13	
8+0				80.38	

Conc to b.

Vert. Spk. W. side twin Elm 25' E. & Bass Lake Rd. & 36' N. & Butternut Rd.

○ = Tang ℄
□ = Occ ℄

W				℄		E		
5.50 / 30	5.20 / 16	5.65 / 13	□ 4.82 / 3	○ 4.90	5.65 / 8	6.15 / 10	5.75 / 12	6.45 / 30
3.42 / 30	4.06 / 15	4.78 / 13	□ 3.62 / 2	○ 3.62	4.22 / 9	4.73 / 11	4.15 / 13	4.70 / 30
9.8 / 30	10.6 / 18	12.8 / 14	□ 11.56 / 2	○ 11.50	12.6 / 8	12.8 / 12	12.75 / 19	10.6 / 31
7.5 / 30	7.15 / 17	8.33 / 14	□ 7.73 / 2	○ 7.76	8.05 / 6	7.8 / 8	6.7 / 30	
6.35 / 30	6.40 / 13	7.12 / 15	□ 6.10 / 5	○ 6.14	6.45 / 6	6.70 / 10	3.8 / 30	
5.67 / 30	6.07 / 13	7.2 / 15	□ 6.95 / 5	○ 6.6	7.2 / 7	7.0 / 9	5.3 / 13	3.7 / 30
3.9 / 30	4.25 / 19	4.9 / 16	□ 4.9 / 5	○ 4.25	5.0 / 7	4.2 / 10	2.5 / 30	
out 5.75 / 25	6.8 / 11	5.9 / 16	□ 4.95 / 5	○ 5.0	5.65 / 7	5.9 / 11	5.7 / 30	

	+	HI		
		1285.38		
9+0				1280.24
B.M. #2	3.28	1285.82	2.83	1282.54 ✓ Elev Corrected
10+0				80.32
11+0				80.72
~~12+0~~ (PC)				
12+00				81.52
+50				81.62
13+00				81.83
T.P. 3	6.48	1289.11	3.19	1282.63 ✓
BM #3			0.48	1288.64 ✓ Elev Corrected
13+50				83.41
14+0				84.81
		Stopped Rain		
BM #3	1.72	1284.36		1282.64 ✓ corrected
+50				84.61
15+0				85.21
+50				1285.41

W — E

6.7/30 6.8/15 5.8/15 5.0/4 5.14 5.75/7 6.65/12 5.5/30

Vert. Spk. NW Side 24" Elm 35' Out ℄ Sta 4+75

out 6.0/24 7.0/20 6.2/18 5.2/4 5.50 5.3/14 6.8/9 5.9/13 4.7/30

5.6/30 5.7/22 4.3/19 5.8/17 5.0/4 5.1 5.7/7 6.3/8 5.4/10 4.1/30

5.3/30 6.0/19 5.5/17 4.6/5 4.7 5.2/7 5.9/8 5.0/11 4.5/14 4.3/30

4.5/30 5.4/19 5.0/16 4.2/5 4.3 4.5/6 5.3/7 4.2/11 3.9/16 3.5/30

3.4/30 4.8/20 4.6/18 3.8/8 4.2 4.4/4 5.0/5 3.8/7 2.5/11 2.5/30

3.0/30 4.2/24 4.1/22 3.2/12 4.0 4.3/1 3.2/3 2.3/11 1.8/30

Vert Spk SE Quaken Aspen 18" Ash

6.8/30 5.9/17 6.5/7 6.8/6 5.7 5.2/12 4.5/30

5.8/36 5.2/24 6.1/13 4.8/10 4.3 3.5/30

6.7/37 5.9/26 6.9/14 5.5/11 4.7/7 4.5 4.2/30

6.2/34 5.4/24 6.3/11 4.1/6 3.9 4.6/13 4.0/30

5.3/30 5.4/26 4.6/15 5.5/3 5.9/2 4.9 4.3/6 4.6/30

		90 1284.36		
TP 4	5.48	1286.10	3.74	1286.62
16+0				85.90
+50				86.50
T.P. 5	5.01	1286.41	2.70	1287.40
17+0				86.91
18+0				88.11
+50				88.01
19+0				87.91
TP 6	5.28	1286.11	7.58	1286.83
+50				88.71
20+0				85.61
+50				82.81
21+0				81.61
+50				80.51
TP 7	3.82	1284.68	11.25	1280.86
22+0				1280.48
B.M. #A			5.01	1273.67

Elev Corrected

W ℄ E

5.9/30 6.1/25 D 6.5/21 □ 5.6/9 ○ 6.2 6.6/4 D 7.0/7 6.5/10 6.9/15 7.3/25 swamp

5.4/30 6.0/22 6.5/20 □ 5.5/10 ○ 5.6 6.2/7 6.9/10 6.3/14 6.6/30 wet

Top SPK Stake Sta 17+40

5.8/30 6.9/19 D 8.7/13 □ ○ 7.5 7.9/9 D 8.7/10 7.6/13 7.8/30

9.6/30 5.7/11 D 7.2/9 ○ 6.3 □ 6.3/3 D 7.2/14 6.0/18 6.4/30 ℄

5.4/30 6.0/7 D 6.9/5 ○ 6.4 □ 5.9/9 D 6.7/20 6.0/24 6.0/30

5.2/30 D 5.2/9 ○ 6.5 D 7.5/2 □ 6.6/14 ○ 7.4/28 6.5/30 6.7/40

3.6/30 3.2/15 ○ 3.7 ✕ 5.6/7 D 7.1/10 □ 5.8/22 6.2/32 D 6.5/33 4.9/40

5.5/30 ○ 6.5 D 8.1/12 □ 8.7/15 7.4/26 D 8.2/38 8.5/40 7.6/50

Drive 9.2/30 ○ 9.3 9.4/20 D 8.8/28 9.4/40 10.1/42 9.0/50

10.3/30 ○ 10.5 D 11.0/6 10.8/8 □ 9.7/18 10.5/30 11.0/33 9.5/40

11.2/30 11.3/6 D 12.4/2 ○ 11.6 □ 11.5/12 ○ 11.9/25 10.1/30

4.7/30 4.7/12 5.7/8 D 4.9/6 ○ 4.2 □ 3.9/8 4.8/19 5.4/20 4.0/30

SPK W.S.12 Root Triple Elm Sta. 22+50 30' Rt ℄

		1278.68			
22+50				80.28	
23+0				79.68	
24+0				79.18	
TP	2.49	1275.17	6.00	1272.68	
25+0				77.67	
26+0				76.07	
27+0				75.47	
28+0				73.87	
T.P.	2.65	1272.27	5.55	1269.62	
29+0				68.57	
TP	0.78	1267.55	9.50	1267.77	
30+0				63.35	
31+0				61.35	
B.M. #5	5.73	1259.09	10.19	1253.36	corrected Rain
31+0				61.36	
+36	18" CIP on 60° Skew 33' long				
32+0				57.16	
T.P.	3.23	1257.14	9.21	1249.88	
33+0				50.98	

5.9/30 5.8/15 6.1/13 5.2/10 4.9 5.4/12 6.3/15 5.8/20 5.8/30

6.0/30 5.7/17 6.5/13 5.6/11 4.8 5.6/12 6.4/15 6.3/30

4.4/30 5.3/20 7.2/14 6.3/10 5.5 6.2/10 7.5/13 6.2/20 6.0/30

Drive 3.20/30 5.27 TL 15" Storm Culvert DI. 6.51 3.5 4.2/10 5.5/15 4.2/20 4.4/30

5.0/30 6.8/15 5.8/12 5.1 5.9/12 6.8/15 6.4/30

6.9/30 7.2/20 8.0/15 6.7/10 5.7 6.4/10 8.1/15 6.9/20 7.1/30

7.7/30 7.4/15 9.8/11 7.9/8 7.3 8.2/12 10.2/17 8.0/20 out

Top Sta 31+0 Sta 28+0

5.3/30 5.4/21 10.2/13 8.7/11 7.7 8.7/13 10.5/15 6.9/22 7.1/30

1.7/30 2.3/18 6.3/11 5.1/10 4.2 5.4/13 6.4/15 4.1/21 3.8/30 out

8.2 9.3/12 10.3/14 9.7/18 10.9/30

SPK. Rd. Face D 30' Rt CL Sta 318295 Sta 314+50

D.I. 5.5/30 3.6/23 5.2/15 5.6/13 4.5/9 3.9

4.0/30 5.2/17 9.3/11 8.6/9 7.9 8.5/11 11.5/16 10.0/20 8.0/30

3.8/30 4.8/22 9.7/13 9.0/11 8.1 9.2/12 12.1/16 8.3/21 8.4/27 8.0/30

		125 9.08 7.11			
T.P. 12	4.50	124 51.85 5.88	11.73	124 7.35 7.35	
34+0				1246.25	
35+0				41.75	
T.P. 13	3.54	123 43.83 7.86	11.56	123 40.29 4.32	
35+50				39.93	
36+00				38.63	
36+50				37.73	
37+00				36.53	
37+50				36.53	
38+00				37.63	
TP 14	6.68	123 44.78 8.81	5.73	123 38.10 2.13	
38+50				39.78	
B.M. #6			5.19	1237.63 9.63	Elev Corrected

Continued on Page 69
this book

W E

3.0/30	3.5/20	D 7.5/13	6.4/12	S 5.6	6.7/12	D 9.4/15	6.4/22	6.6/30
8.3/30	8.7/20	D 12.1/12	11.2/10	S 10.1	10.9/11	D 12.9/17	9.2/27	9.7/30
3.6/30	3.9/19	S 5.7/14	5.0/11	S 3.9	4.5/10	D 7.8/18	4.2/23	4.5/30
5.6/30	6.0/18	D 6.6/15	6.2/11	S 5.2	6.0/10	D 7.8/16	8.9/26	8.3/30
6.7/30	7.1/17	D 8.3/19	7.3/11	S 6.1	Drive 6.0/10			4.7/30
7.7/30	8.6/17	9.4/15	7.7/10	S 7.3	8.4/11	8.9/21		10.0/30
7.3/30	7.9/16	8.6/14	8.0/11	S 7.3	8.6/11	8.0/13		9.0/29
5.8/30	Drive	6.9/11		S 6.2	7.0/11	Drive		6.5/30
A.1/30	3.6/20	D 6.6/13	6.9/10	S 6.0	5.8/12	Drive		A.5/30

Spk. Rd. Face C.E.I. # 577799 Sta. 39+30 30' E of ℄

434.7
1406.1
1840.8
153.2
1994.0
134.5
2128.5

~~76°05'~~
~~42°07'~~
~~33°58~~
76°05'20"
42°06'40" 5°52'
33°58'40"
76°05'20"
83° 01'20"
159 6'40"
200 53'20"
42°06'

180°00'
47°15'
132°45'

53°15'20"
74°23'20"
127°38'40"
52 21'20"

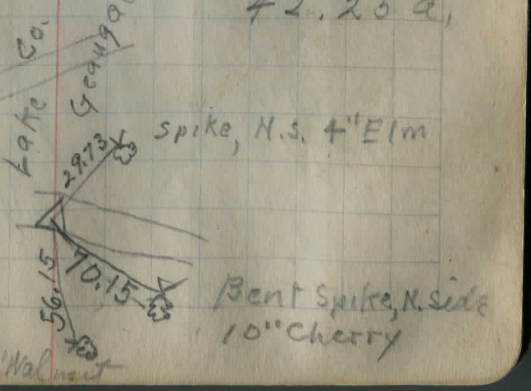
Ch. 27 Tinning Rd

26

CHARDON-MUNSON Town Line Road.

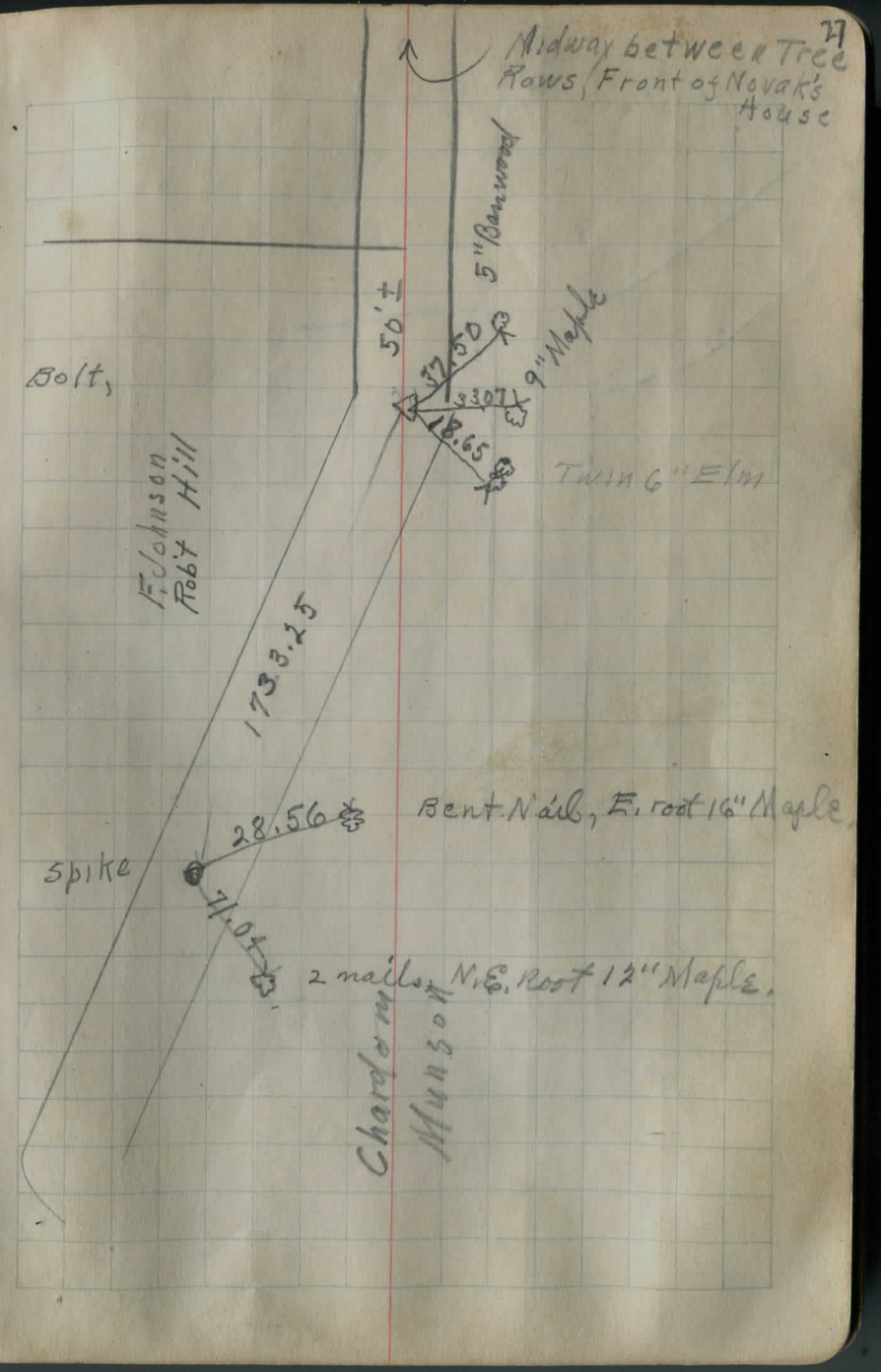
V. 177 - P. 213.

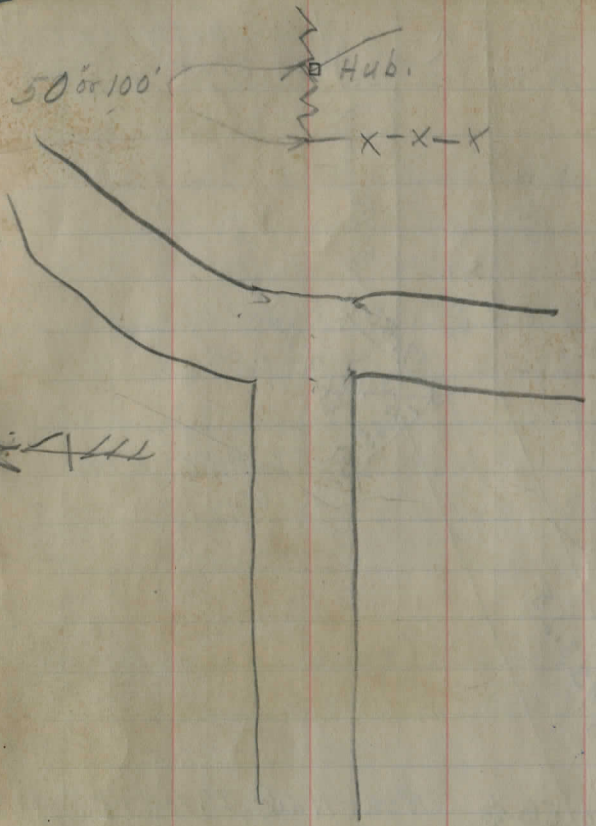
- Newton Heath to M.B. McLaughlin bg. at a pt. in ℄ Ch.-Euc. Rd at N.W. Cor of lands in Lots 158-164, C.C. Pratt + L.C. Murray
- S 79°38' W along ℄ 739.2' to angle point
- S 70°24'45" W along ℄ 406.0 to W. line Lot 164
- S 5°09' W. along lot + County line 379.9' to ℄ Clark Rd.
- S 42°06'40" E 434.7
- S 76°05'20" E 1406.1
- N 83°01'20" E. 153.2'
- N 64°36' E. 134.5
- N 53°15'20" E, 267.1' to
- S.w. ly cor. H.D. Pratt to D.W. Bailey
- N 3°56'40" E. along W. ly line 693.3'
- N 86° 14'20" W 354.7'
- S. 0°16'20" W. 110.2'
- N. 84°58'20" W. 733.9'
- N 5° 06'40" E 404.7' to p.b., 42.25 a.



170-382 A.D.+G.M.Platt to D.W.Bailey
part of lot 164, Tr. 3,
bg. at point in ℄ Clark Road, 2970' N.W.ly,
from S.E.ly. cor. 102 66/100 a,
N. 5° E along W.ly line 102.669,
1080.8' to N.C.Bartlett
- N. 86°14.7' W 1421.8
- S.3°56.6'W 693.8
- S 74°23 11/30' E along ℄. 915'
- S. 64°37 1/3' E along ℄, 541.6 p.b. - 27.83 a.

173-65 J.+M.Valroda to C.N.+L.L.Curtis
bg. in ℄ road at N.E. cor. Harry Gunn
- N 60°56'E 134.5'
- N 50°23'E. 167.3'
- N 72°41'E. 168.0'
- S 82°06'E 215.9'
- S 77°25'E. 431.15'
- S 72°37'E 412.75'
- S 67°56'E 268.6' to N.W. cor. J.+E. Hulda
- S 0°14'E passing through iron stake at 23.94', 1737.3' to a marked brick stone Twp. line.
- W. along Twp. line 933.1 ft. to iron stake
- N. 0°34'E, 391.1' to p.b. — S. 89°02'W, 838.1'
- N 2°35'E 1470.0' to p.b., passing through iron stake 28.6' from p.b. 69.951





Apr. 6, 1927

Marks, Grau, Snyder

2129.5
266.75
2395.25

11°20' Left. Spike Head in 5" Elm 30.2 — 30' — Hub. — 21+28.5

90° 90°

134.5

90°

18°25' Left — 30' — 30' Hub, Hub — 19+94.0

Spike + Roofing Cap in 16" Maple — 76.0

Δ = 20°53' Left — 18+40.8'

Spike + Roofing Cap in 24" Beech — 60.0

See this book pg 74 For May 1952 references

Δ = 33°59' Left

Nail + Tin Cap 10" Walnut (Dead) — 24.5

33°59'

21.5 — 4+34.7 Iron Pipe

Nail + Tin Cap, 6" Thorn Apple

32.0

Nail + Tin Cap 15" Walnut

Iron Pipe — Cleveland & Chardon Road — Chardon TWP 132.64.5' — Stake — Kirtland TWP.

45+00 Hub. 0°00'

P.T. 34+04.3 4°53'
34+00 4°48'
33+00 2°48'
32+82.5 P.I. Δ = 9°46' Right
32+00 0°48' D = 4°00' T = 122.4 L = 244.2
31+60.1 P.C.

25+56.0 P.T 26°10'
25 21°52'
24 14°24'
23+95.25 P.I. Δ = 52°20' Right
D = 15°00' R = 383.07 T = 188.15
23 6°52' L = 348.9
22+07.1 P.C.
34+8.9
25+56.0

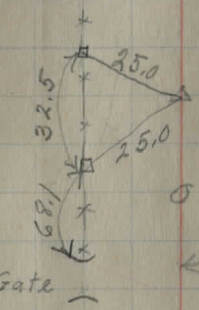
79.1

Hub 25' 90°

10957

12-15-07
I.P. fd & ref
See PG 75

90°
Hub. 25'



Hub, Sept. 21, 1927
Iron Pipe

25' Hub.
90°
Stopped Apr. 7, 1927
Marks, Grace, Snyder.

90°
Hub Spike

△ Iron Pipe, S.W. Cor. D.W. Dailey

Hub. 25' Spike
90°

86+61.3 10°40½' P.T.

86 7°37'

85+55.8 P.I. Δ = 21°21' Left

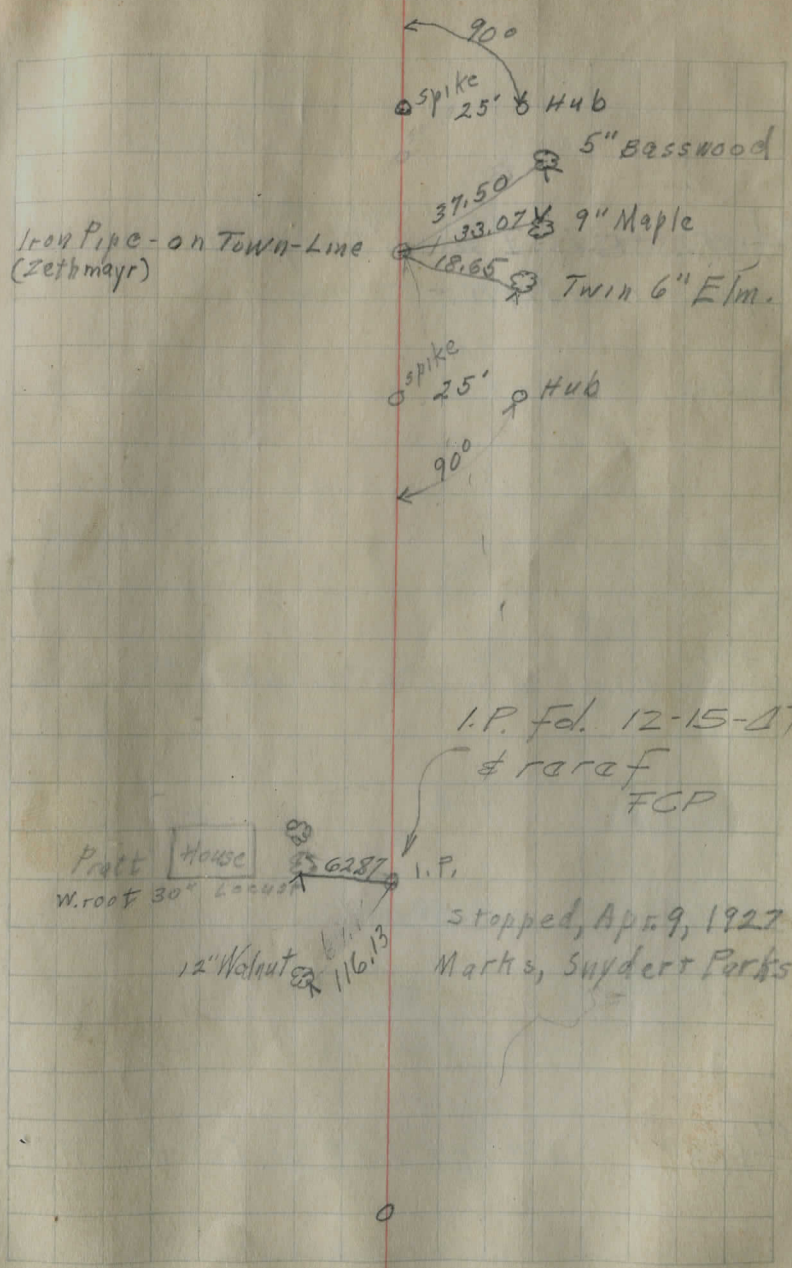
D = 10°00' – T = 108.0 – L = 213.5'

85 2°37' E = 10.09±

84+47.8 P.C.

63+00 Iron Pipe Δ = 0°21' Left

50+00 Hub. 0°00'



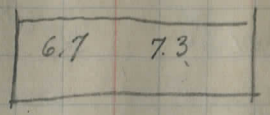
~~141~~ 141 ~~+95.2~~ Steel I Beam Bridge, Total Length 18.0', Clear Span 15.5'
Good Condition

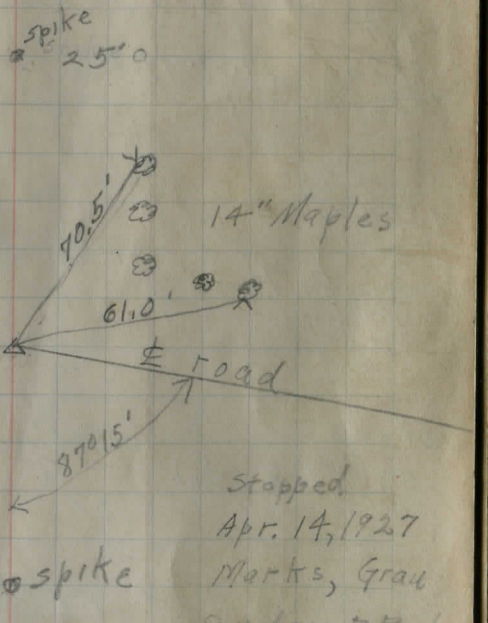
~~130~~ 130
~~+92~~ +00

122+68.0
~~+24~~ +68.0 P.I. Δ = 0°10' Left

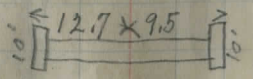
~~119~~ 119
~~+50~~ +70 Δ = 0°00'

~~99~~ 99
~~+01~~ +89.2 42" Corr. Iron Pipe, Concrete H.W.S.





Stopped
Apr. 14, 1927
Marks, Grau
Snyder, D. Parks



May 1, 1928, Discovered that in original Survey Sta. 87 had been erroneously marked "89", and this 200' error had been carried through.

185+99.5 (S-4)

186+00
~~188~~ 100 0°00'

See back of book for new ref. pg 77

179+01.64

179+00
~~181~~+00 0°00'

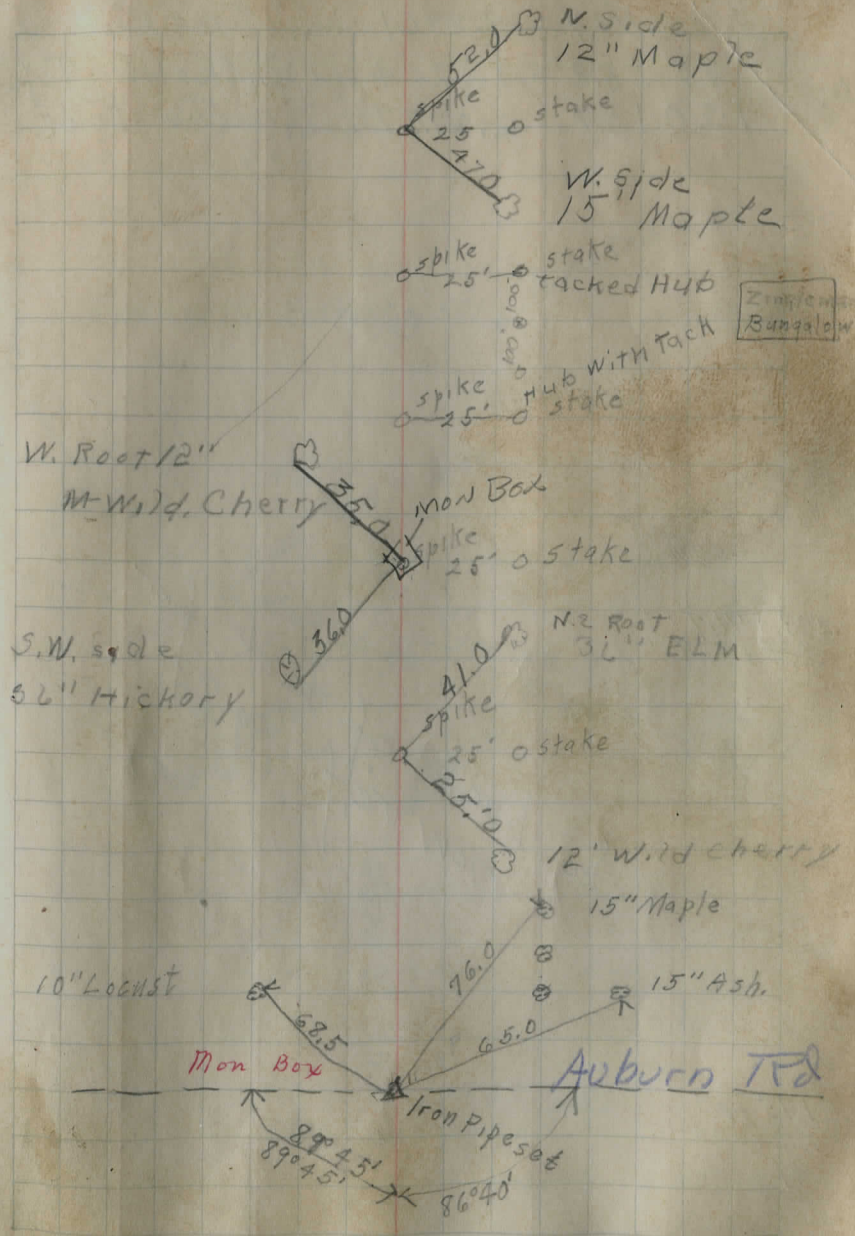
178
177

171+00 170+99.85
~~173~~+00 0°00'

166+00
~~168~~+00 0°00'
166+00.90 (S-2)

159+00 0°00'
158+99.8 (S-2)

151+75.0
~~153~~+75.0 ± N. & S. Center Road. Δ = 0°03' Left

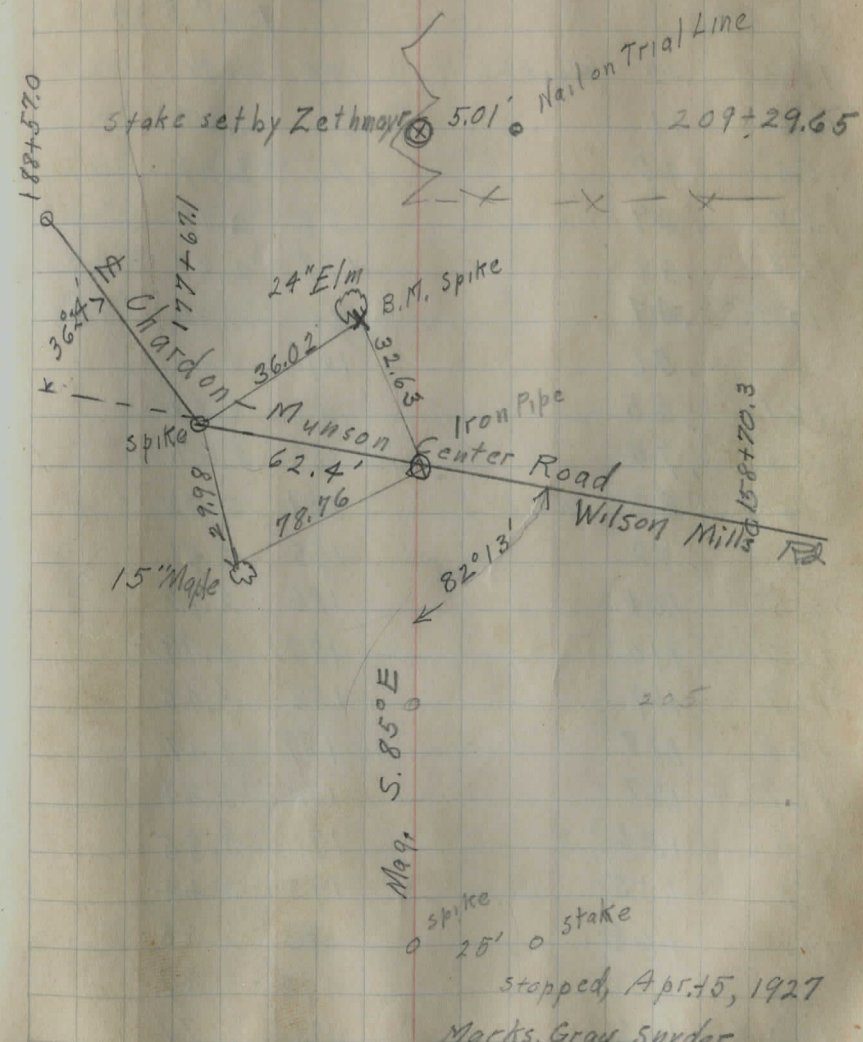


(203+71.7) = 3.8558 mi
205 71.7 = 3.8961 mi. Total Distance
85 55.8 = 1.6204 mi in Chardon Twp
120 15.9 2.2757 mi. on Town Line

203+71.7
~~205~~+71.7

195+00
~~197~~+00

See back of book for new ref. Pg. 78



Stopped, Apr. 15, 1927
Marks, Graul, Snyder.

430
.009
.3870
5.01
39
4.62

20929.5
153.75
5554.5

.000982

5.01000
499905
1095.00

154	.02	North.
155	.11	
156	.20	
157	.29	
158	.38	
159	.47	
160	.56	
161	.65	
162	.74	
163	.83	
164	.92	
165	1.01	
166	1.10	
167	1.19	
168	1.28	
169	1.37	
170	1.46	
171	1.55	
172	1.64	
173	1.73	
174	1.82	
175	1.91	
176	2.00	
177	2.09	
178	2.18	
179	2.27	
180	2.36	
181	2.45	
182	2.54	
183	2.63	
184	2.72	
185	2.81	
186	2.90	
187	2.99	
188	3.08	
189	3.17	
190	3.26	
191	3.35	
192	3.44	
193	3.53	
194	3.62	
195	3.71	
196	3.80	
197	3.89	
198	3.98	
199	4.07	
200	4.16	
201	4.25	
202	4.34	
203	4.43	
204	4.52	
205	4.61	

No structure present,
205+00 - 12 or 15" Pipe required

192+23 12" - 2 piece segmental C.I. Pipe

186+66 12" Vit. Pipe.

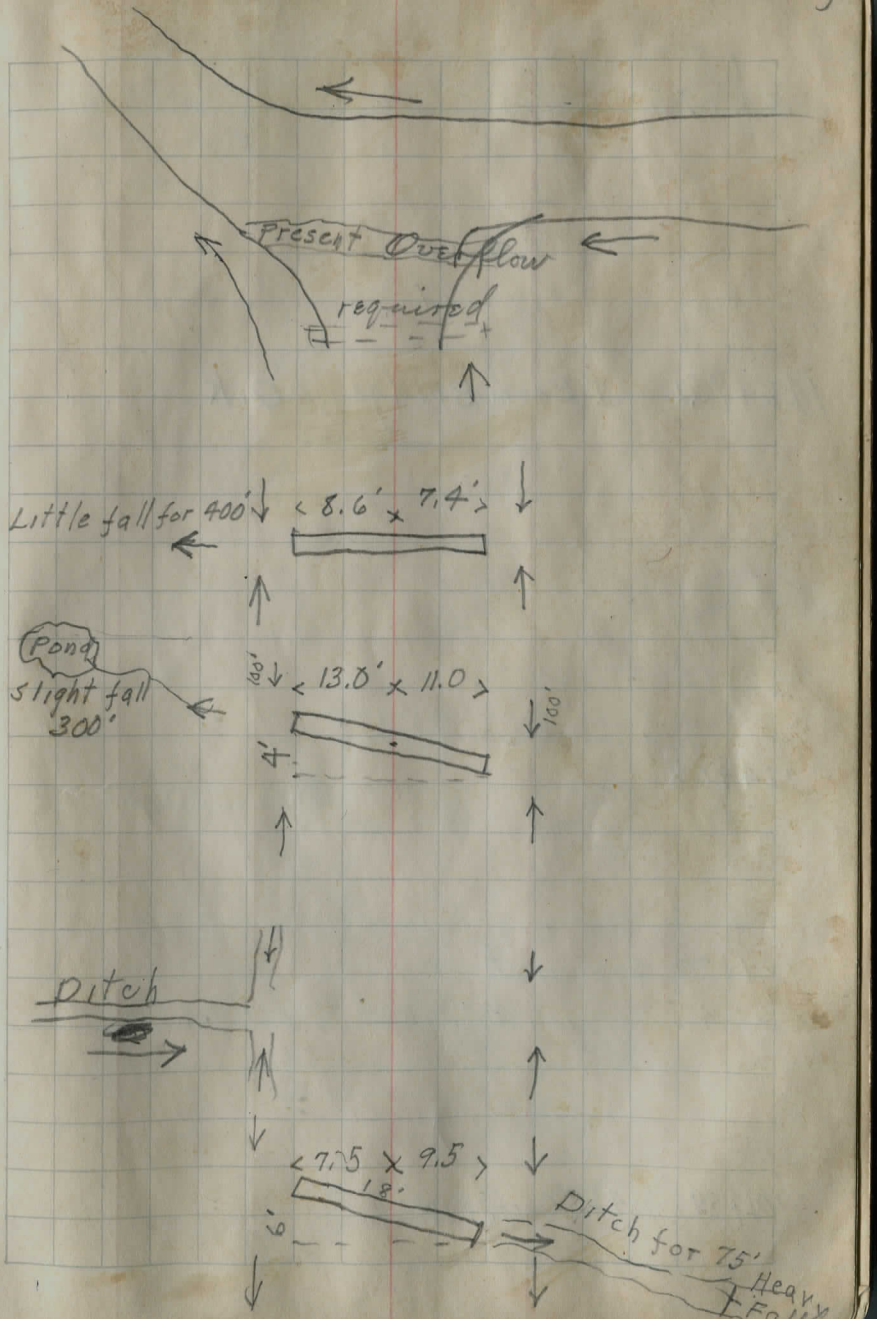
176+50 Summit

174+40 12" Pipe required

173+00 (?) Summit

(160+82 (!))

162+82 12" Solid C.I. Pipe



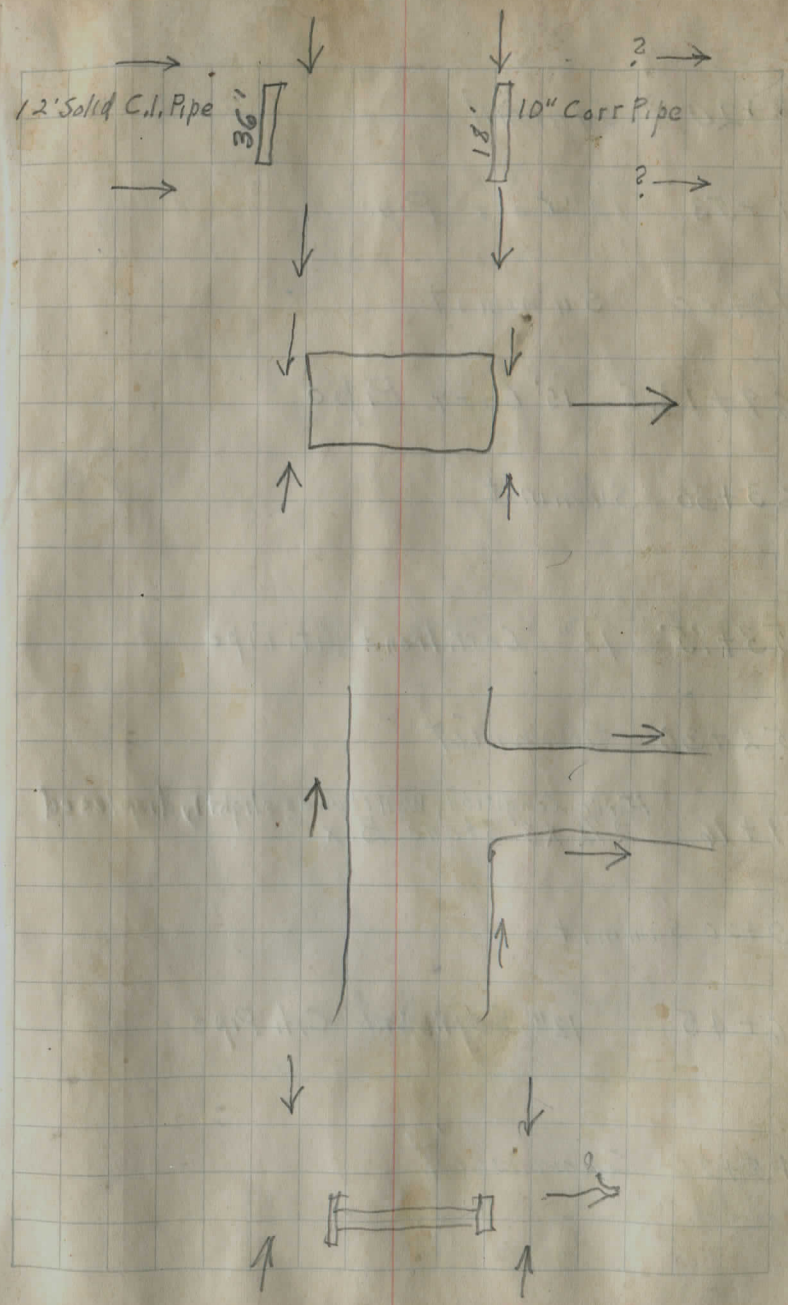
15 1/2 + 75

143 + 95.2 I Beam Bridge, O.K

124 + 68

121 + 70 Summit

101 + 89.2 42" Corr. Pipe



83+20 Summit,

71+53 12" Corr Pipe

70+00 Summit

69+13.5 15' Corr. Pipe

63+36 Summit

53+95 12" Corr. Iron + Vit. Pipe

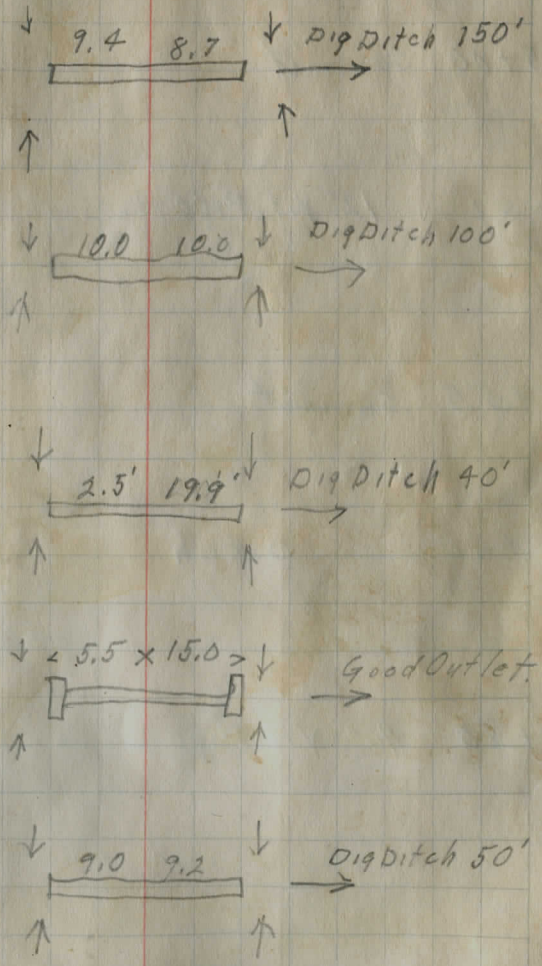
52+30 Summit

51+16 Fair Condition, Wallstones slightly displeced
2½ X 3' Stone Box

50+20 Summit

46+45 12" ~~Segment~~ C.I. Pipe

45+20 Summit



stopped Apr. 16, 1927 - Rain
Marks, Grau, Snyder, D. Parks.

37+82 7' x 4.3' Concrete Culvert
Good Condition

35+00 Summit

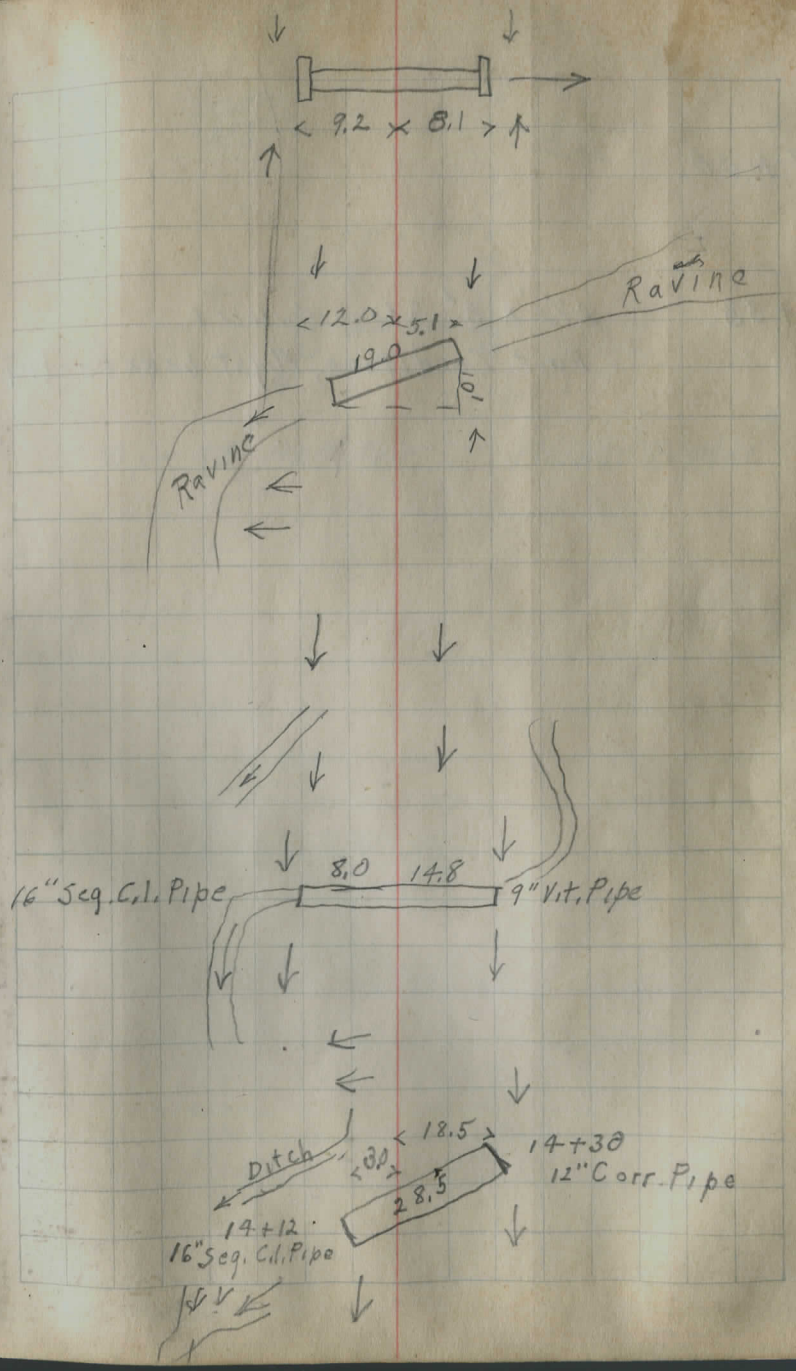
31+81 12" Vit. Pipe

27+55 Summit

24+40 Ditch

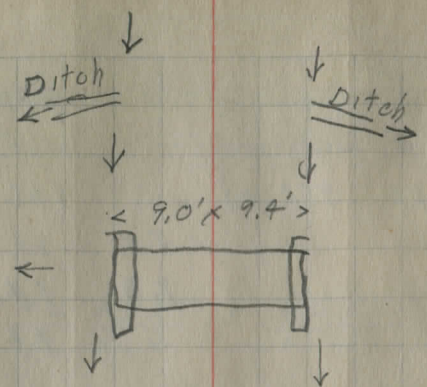
20+85 9" [illegible]

14+12 - 14+30.



7+00

5+33 2½' X 3' Stone Culvert
Fair Condition, Might be extended to North.



Apr. 18, 1927 Fair. Marks-Snyder A.M

B.M.				948.73
B.M.				1285.36
B.M.	1.30	950.03		948.73
0-200			7.8	942.2
0-10			7.3	942.7
0+00				943.6
1+00				947.2
	11.97	961.58	0.42	949.61
2			10.9	950.7
3			6.3	955.3
4			1.6	960.0
+33 T.P.	12.08	973.64	0.02	961.56
5			6.0	967.6
5+33				972.3
T.P.	10.19	983.23	0.6.0	973.04
6			5.3	977.9
	11.89	994.89	0.23	983.00
7			2.9	992.0
	11.62	1005.63	0.88	994.01
	12.44	1017.18	0.89	1004.74
8			11.6	1005.6
	12.69	1029.49	0.38	1016.80
9				1019.7

E. root, 14" Hickory 70' W. of County line, 40' N. of E. of I.C.H. 34
W. Root, 14" Elm, E. of Gravel Road, Burdicks. Corner,

3.5/25 3.5/19 4.2/18 4.5/6 5.3/2 6.4/0 5.4/3 5.3/8 6.1/16 4.4/18 4.5/25

0.0/25 2.0/9 2.6/7 2.2/3 2.8/2 2.8/0 2.6/4 2.9/11 1.0/15 1.3/25

5.8 2.7 - 0.8 / 9.4 1.3 / 7.0 0 7.0 0.5 - 2.2 5.2 / 9.4

S.W. cor. N.H.W. Culv. 5+33

6.7/30 4.0/25 3.0/22 4.0/17 5.8/13-12 5.3/11 5.3 6.6/25 8.1/29 8.3/34 8.0/40 2.0/48

14.0/4.0 13.0/33 8.8/25 1.5/15 3.0/12 2.9/0 2.7/7 1.8/8.5 2.9/13 5.6/17 0.0/27 1.0/35

9.5/45 6.7/35 5.1/25 12.5/17 11.8/16 11.6/0 11.6/8.5 12.9/10 2.0/22-30

6.4/3.5 5.5/25 11.2/18 7.7/8 9.8/0 10.5/6.5 11.4/8 9.4/9 1.1/20 0.8/25 0.3/35

		1029.49		
	12.29	1041.51	0.27	1029.22
10				1032.1
	11.93	1052.95	0.49	1041.02
11				1041.9
	12.40	1063.85	1.50	1051.45
12				1051.2
13				1056.9
	8.90	1072.32	0.43	1063.42
14				1064.9
+30			3.6	1068.7
B.M.			0.03	1072.29
	11.21	1083.50		
15				1072.3
	12.72	1095.76	0.46	1083.04
16				1081.3
17				1088.8
	12.36	1107.19	0.93	1094.83
18				1096.3
19				1102.5
	9.18	1116.24	0.13	1107.06
20				1108.8

6.0/30 5.9/25 7.4/16 10.5/12 9.2/3 9.4/0 9.9/8 10.7/9 2.7/20 1.9/30

8.3/35 7.5/25 6.8/14 11.7/8 11.1/6 10.6/0 11.1/12 12.0/14 4.9/23 3.7/30 2.9/35

11.9/30 11.6/25 10.7/18 12.2/11 14.5/9 13.5/7 12.7/0 12.9/9 14.0/16 7.9/25 7.5/35

21.0/50 18.0/40 10.8/25 5.5/12 5.1/4 7.3/2.5 7.0/0 6.4/7 7.2/19 7.8/21 4.8/26 1.4/34 0.0/45

13+85 18.0/30

13.0/30 11.9/23 8.4/16 13.0/11 7.4/0 6.2/4 6.4/27 2.1/33 1.1/40

Spike in E. side of 20" stump, 33'5.0 ± E, 14+12

8.9/35 8.2/25 7.0/11 9.3/5 12.3/2 11.3/0 10.6/6 11.2/14 12.2/17 9.4/18 4.4/30 4.0/35

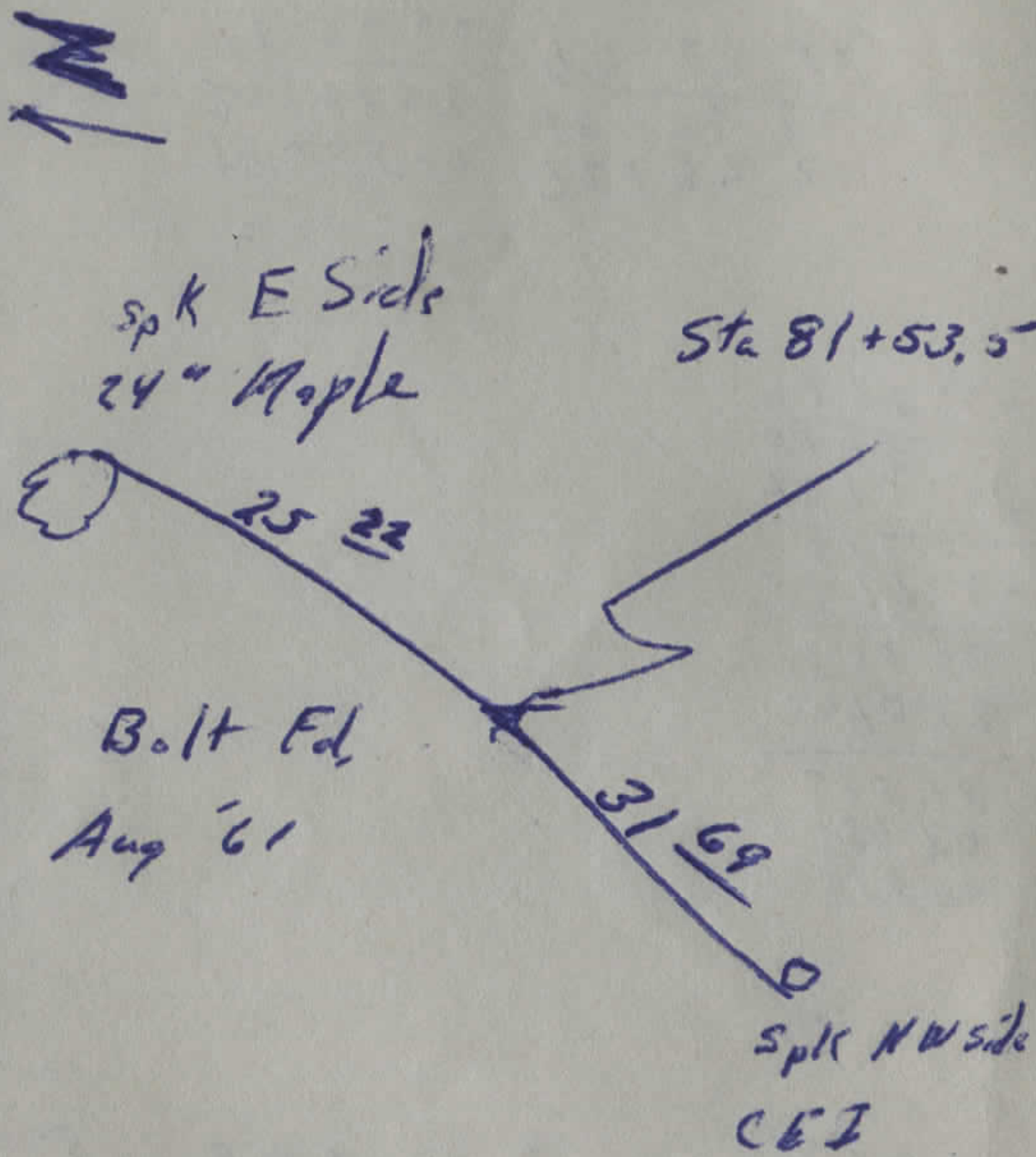
12.0/35 11.6/25 11.2/12 12.2/9 15.5/4 14.6/2 14.5/6 14.2/13 15.5/15 14.0/17 10.3/27 9.6/35

6.3/35 4.8/10 7.5/5 7.0/3 7.0/0 6.9/6 7.4/11 8.3/13 2.8/19 2.0/35

4.5/35 11.0/25 10.4/8 11.9/7 11.5/6 10.9/0 11.2/7 11.8/9 12.4/10.5 10.3/12 7.2/18 6.0/30

5.0/35 3.9/17 3.2/5.5 5.1/4 4.7/0 4.1/4.5 4.4/10 4.9/13 5.8/14.5 4.6/16 0.0/25 +2.0/35

16.5/35 16.0/30 13.2/25 6.4/12 8.4/9 8.0/7 7.4/0 7.6/10 8.1/12.5 5.2/16 4.7/20 4.0/30


N
Spk E Side
24" Maple
Sta 81+53.5
25 22
B.lt Fd
Aug '61
31 69
Spk NW side
C&I

		1116.24 ✓		
21				1112.0
	9.69	1125.77 ✓	0.16	1116.08 ✓
22				1118.2
	12.34	1137.26 ✓	0.85	1124.92 ✓
23				1126.2
	11.90	1147.88 ✓	1.28	1135.98 ✓
24				1135.5
25				1145.1
	12.67	1160.42 ✓	0.13	1147.75 ✓
26				1152.1
27				1157.4
+60			0.6	1159.8
28			2.0	1158.4
29			1.7	1158.7
+25			1.5	1158.9
30			2.2	1158.2
31			2.9	1157.5
	12.06	1169.02 ✓	3.46	1156.96 ✓
32			11.7	1157.3
33			8.3	1160.7
34			4.0	1165.0

6.4/25 6.3/20 4.0/7 — 4.2/0 — 4.0/4 — 4.4/10.5 — 5.3/11.5 — 4.3/15 — 4.0/25

4.5/35 — 4.2/25 — 4.1/14.5 — 6.2/10 — 8.8/8 — 7.6/0 — 8.2/5 — 9.1/7 — 6.1/9 — 6.0/14 — 8.7/19 — 9.1/28 creek — 8.0/35

9.1/35 — 7.8/9.0 — 11.9/6 — 11.1/0 — 10.7/2 — 11.0/9 — 11.7/11 — 9.7/13 — 9.4/15 — 8.0/18 — 8.3/22

14.5/35 — 15.5/45 creek

10.4/35 — 9.7/15 — 11.9/8 — 12.7/7 — 12.4/0 — 12.9/1 — 13.6/8 — 9.2/13 — 9.3/20 — 13.1/31 — 22±/50± creek

4.9/35 — 0.7/17 — 3.9/11 — 2.5/3 — 2.8/0 — 3.5/5 — 1.3/7 — 0.0/12 — 1.9/28 — 8.4/43 — —/50± creek

6.9/35 — 5.6/19 — 7.0/16 — 8.8/14.5 — 7.6/6 — 8.3/0 — 8.7/1 — 6.6/3 — 4.8/12 — 6.3/27 — 9.0/35 — 22±/50± creek

1.8/25 — 1.8/16 — 3.2/14 — 2.5/7 — 3.0/0 — 3.2/1 — 2.1/2.5 — 3.7/25

		1169.02		
35			1.2	1167.8
+20			1.6	1167.4
+70			7.1	1161.9
36			9.2	1159.8
37			13.5	1155.5
38			13.6	1155.4
39			11.0	1158.0
40			4.6	1164.4
	11.69	1179.29	1.42	1167.60
+60			8.5	1170.8
41			6.0	1173.3
42			1.3	1178.0
	10.00	1189.06	0.23	1179.06
43			8.0	1181.1
44			5.0	1184.1
45			2.5	1186.6
+30			1.7	1187.4
46			4.0	1183.1
47			5.4	1183.7
B.M			2.70	1186.36
48			2.7	1186.4
			0.64	1188.42

Spike, S.W. Root, 40" Bitter-nut, N. of 46+90
Cut Area 0.0 sq. ft.

	10.35	1196.71		1186.36
49				1189.9
	12.95	1209.69	+0.03	1196.74
50				1199.8
+35				1200.6
50+75			11.4	1198.3
	13.03	1209.77	12.95	1196.74
51			11.4	1198.4
+65			11.1	1198.7
52				1202.0
+35			7.1	1202.7
53			7.8	1202.0
54			8.1	1201.7
55			4.4	1205.4
+60	12.09	1220.74	1.12	1208.65
56				1212.2
+50			2.0	1218.7
	12.95	1233.60	0.09	1220.65
57				1222.2

May 9-1927 Marks, Gray, D. Parks

4

Left 46+90

1.6/25 4.0/11 6.1/2.5 7.2/1 6.8/0 6.2/6 6.8/13 7.3/14 5.9/15.5 5.2/25

0.5/35 11/25 2.0/12 9.6 10.1/0 9.9/5.5 9.4 2.3/13.5 2.3/35

+1.0/35 1.9/12 10.0/2 9.7/0 9.1/4 9.8/10 2.5/16.5 1.6/20 1.5/35

Cut Area 0.0 sq. ft.

Cut area 0.0 sq ft.

1.7/35 2.4/25 11.5 7.8/0 9.5/2 9.0/9 9.4/15.5 6.5/22 6.7/25

Cut Area 0.0

3.0/35 3.8/25 5.0/13 6.3/6.5 7.7/4 9.7/2 8.5/0 7.6/6.5 8.1/16 8.7/18 7.0/20 6.4/23.5 25

4.0/35 5.0/25 7.0/10 9.0/4.5 12.1/1.5 11.4/0 10.2/7.5 11.1/14 11.9/16.5 9.7/18.5 8.5/25 8.7/35

		1233.60		
	12.76	1244.82	1.54	1232.06
58				1231.9
+50			6.5	1238.3
	11.48	1255.11	1.19	1243.63
59				1243.1
60				1247.4
	12.98	1267.54	0.55	1254.56
61				1258.0
	8.53	1274.62	1.45	1266.09
62				1266.2
63				1270.0
			0.74	1273.88
+45			3.8	1270.8
64			6.1	1268.5
65	2.6	1267.3	9.9	1264.7
66			6.6	1260.7
67	3.5	1259.2	11.6	1255.7
68			8.5	1250.7
69			10.5	1248.7

4.5/35 5.0/25 6.1/11 13.7/1

12.9/0 12.2/7 12.5/13.5 13.2/15 8.8/18 8.4/21.5 8.7/25 9.2/35

7.7/35 8.3/25 9.9/7.5 12.8/4

12.0/0 11.4/5 12.3/12.5 13.1/14 11.1/15 11.0/25 11.8/35

1.0/35-25 4.0/10 6.5/7 6.0/5.5

5.7/25 5.5/2.5 6.4/9 7.0/11 5.2/12.5 4.5/17 5.5/35

6.3/35 6.5/25 6.4/18 6.9/15 10.3/9.5

9.5/0 10.1/8 7.0/10.5 7.1/25-35

7.1/35 6.7/25 7.3/13.5 8.2/10.5 9.7/9.5 8.9/7.5 8.4/0 9.2/6 9.6/7 6.8/9 5.9/15 6.2/35

3.2/35-15 3.7/10.5 4.8/8.5

4.6/0 5.3/8 4.7/9 4.8/25 5.3/35

House

B. M.-Bent R.R. spike, W. root, W. ly Locust Tree, Front of Pratt's

	2.44	102.44	100.00
35			
36			
37			
38			
39			
40			

P.M. June 13, 1927, Marks, D. Parks, Hassel

Subgrade	Gr. Rod	Ditch Grade	Gr. Rod	Cut (From Top of stake)
99.00	3.44	95.6	6.8	4.2
98.00	4.44	95.2	7.2	4.0
98.00	4.44	94.8	7.6	3.7
98.00	4.44	94.4	8.0	3.5
98.00	4.44	94.0	8.4	3.5
98.50	3.94	93.6	8.8	4.0

B.M 63	0.38	1274,26		1273,88	1271.0
62					1267.4
61					1259,6/4
T.P. 60	0,52	1268,65	16,13	1258,13	1251.8
59					1244,0
	2,07	1245,26	15,46	1243,19	
58					1234.5/7
	0,62	1231,49	14,39	1230,87	
57					1227.5.0/4.9
56					1215,5/8
T.P	7,70	1221,29	14.90	1216,59	
T.P.	3,88	1211,76	13.42	1207,87	

Sept. 7, 1927 P. Parks C. Rand

3,26	3,12	C0,1 / 20,0		4,80	F1,0 / 18,0
6,86	6,70	C0,5 / 20,0		5,16	C1,4 / 22,0
14,86	13,11	C1,9 / 22,0		13,22	C1,6 / 20,5
6,85	5,49	C1,4 / 20,0		7,72	F0,9 / 17,5
14,65	11,83	C2,8 / 23,0		16,00	F1,4 / 14,0
10,96	5,23	C5,7 / 27,5		12,46	F1,5 / 15,5
6,59	2,78	C3,8 / 24,0		9,36	F2,8 / 15,5
16,19	14,87	C1,3 / 21,0	5,79	7,08	F1,1 / 16,5

		1211.75			
52					1202.00
T.P.	8.17	1212.31	7.21	1204.14	
60					1201.00
T.P.	0.34	1198.77	13.88	1198.43	
49					1194.00
B.M.			12.59	1186.18	

Sept. 7 1927 C. Rand. D Parks

		C6.1			F1.8
9.75	3.68	23.0		11.50	15.5
					C6.4
11.31	3.45	27.0		4.89	20.0
2.45					F3.1
		C0.2			17.5
4.77	4.62	19.0		7.82	

	6,34	1078,68		1072,29	
15					1074,3
T.P.	10,98	1089,41	0,20	1078,43	
16					1081,8
T.P.	7,06	1095,04	1,41	1088,00	
17					1089,4
T.P.	6,85	1101,68	0,23	1094,83	
18					1097,2
TP	3,49	1102,31	2,86	1098,82	
19					1102,5
TP			1,17		
20					1103,5
21					1111,3
22					1129,7
23					1121,0
24					1138,0
25					1146,3
26					1153,0

		C1,3		F2,7
4,84	2,71	21,5	4,71	15,5
		C2,8		C0,8
7,61	4,78	23,0	6,85	17,0
		C1,2		C4,4
5,66	4,48	21,0	1,29	24,0
		F0,2		C5,8
5,31	5,51	19,0	0,30	24,0
		21,0		21,5
		18,0		24,0
		17,0		16,0
		21,0		14,0
		20,0		20,0
		20,5		20,5
		20,5		21,0
		22,5		22,0

27 1158,0

20,5 18,0

Sept. 10 1927 D. Parks C Rand

S.W. Corner N. H.W. Culvert 5+33 12

B.M	10.31	983.35		978.04
6				981.3
T.P.	12.16	994.74	0.77	982.58
7				994.2
T.P.			1.43	
8				1007.5
9				1020.5
10				1032.3
11				1042.7
12	5.4 / 3.82 / 1.58			1051.5
13				1059.2
14				1066.8

2.05	3.89	F1.8 / 17.5	7.10	F3.7 / 19.0
0.54	1.16	F0.6 / 15.5	6.35	F5.8 / 19.5
		17.0		31.0
		17.5		31.5
		23.5		29.5
		23.5		14.0
		22.0		16.5
		14.0		16.0
		17.5		18.0

W.C. Marks

Sept. 10, 1927 P. Park S&C, Rand

S.W. Cor., N. H.W. Calk. 5+33

	11.78	984.82		973.04	
6					981.5
	13.06	997.48	0.40	984.42	
7					994.5
	12.84	1009.93	0.39	997.09	
	9.03	1017.58	1.38	1008.55	
8					1007.50
	12.34	1029.37	0.55	1017.03	
9					1020.5
	12.11	1041.03	0.45	1028.92	
10					1232.5
	11.35	1052.04	0.34	1040.69	
11					1043.37
	8.28	1059.82	0.90	1051.14	
12					1052.0
13					1059.5
	10.62	1069.72	0.72	1059.10	
14					1067.0
	6.02	1074.05	1.69	1068.03	
BM			1.72	1072.33	
T.F.	1.72	1074.11		1072.29	Rec
	11.36	1085.06	0.41	1073.70	
15					7074.5

3.32	5.3	F 2.0 / 17.0	7.2	F 3.9 / 19.0
2.98		F 0.9 / 15.5		F 6.1 / 19.5
10.08		F 2.1 / 16.0		C 8.4 / 31.0
8.87		F 1.6 / 17.5		C 8.8 / 31.5
8.53		C 3.5 / 23.5		C 8.1 / 29.5
8.67	6.84	C 2.4 / 23.6	9.25	F 0.6 / 16.0
7.82	6.65	C 1.2 / 22.0	9.35	F 1.7 / 16.5
8.32	1.93	F 1.6 / 14.5	2.60	F 2.3 / 16.0
2.72	5.97	F 3.3 / 17.5	3.66	F 0.9 / 18.0
10.56	9.00	C 1.5 / 21.5	13.02	F 2.5 / 15.5

		1085.06			
16					1082.0
	11.94	1096.66	0.34	1084.72	
17					1089.5
	7.55	1102.51	1.70	1094.96	
18					1097.0
	9.94	1111.35	1.10	1101.41	
19					1102.75
	9.29	1118.00	2.64	1108.71	
20					1108.50
21					1114.25
	9.63	1126.97	0.66	1117.34	
22					1120.81
	11.16	1136.28	1.85	1125.12	
23					1129.00
	10.57	1143.22	3.63	1132.65	
			6.12	1137.10	
24					1138.00
	9.84	1152.77	0.29	1142.93	
25			7.1	1145.7	1147.00
	10.15	1162.44	0.48	1152.29	
26					1153.00
27					~~1159.00~~

3.06	0.31	C2.7 / 23.0	2.38	C0.7 / 16.0
7.16	5.97	C1.2 / 21.0	2.77	C9.4 / 24.5
5.51	5.59	F0.1 / 19.0	0.36	C5.2 / 24.0
8.60	8.00	C0.6 / 21.0	5.64	C3.0 / 21.0
9.50		F 0.3 / 18.0	C3.8 / 24.0	
3.75		F3.1 / 17.0	F 2.0 / 16.0	
6.16		C 1.4 / 21.0	F0.8 / 14.0	
7.28		C0.3 / 20.0	C0.5 / 20.0	

CW. End of Iron Fence

B.M. Concrete Block, S. side of Post, L. 23+80

5.22	F0.4 / 20.5	C 0.4 / 20.5
5.77	C 0.6 / 20.5	C 0.3 / 21.0
9.44	C2.2 / 22.5	C2.3 / 22.0
~~3.44~~	~~C0.4 / 20.5~~	~~F1.2 / 18.0~~

Profile on Sub-Grade

					Finish Grade
B.M.	0.70	1274.58		1273.88	
63			4.2	1270.4	1271.0
62+30			6.1	1268.5	1268.5
62			7.8	1266.8	1267.4
61	0.52	1259.26	15.84	1258.74	1259.6
60			8.6	1250.7	1251.8
59	0.37	1243.45	16.18	1243.08	1244.0
58			9.9	1233.6	1234.5
	1.79	1228.85	16.39	1227.06	
57			4.7	1224.2	1225.0
56			14.3	1214.6	1215.5
	5.50	1164.90		1159.40	
27				1158.25	
27+60				1159.00	
28				1159.00	

Oct. 11, 1927, Marks, D. Parks.

Finish Sub Grade	
1270.3.	
1267.8	
1266.7	0.1' Low
1258.9	0.2' low
1251.1	0.4' low
1243.3	0.2' low
1233.8	0.2' low.
1224.3	0.1' low.
1214.8	0.2' low

May 16, 1928 Marks Rand.

Left Slope Hub, 27+00

6.65 C 1.2 / 20.5

5.90 C 1.5 / 23.0 C 0.8 / 20.0

5.90

	+		−		
B.M.	12,03	1084,32		1072,29	
16					1081.5
T.P.	6.04	1078.06	12,30	1072.02	
15					1074.0
14					1065.0
T.P.	0.60	1062,52	16,14	1061,92	
13					1056.0
12					1047.0
T.P.	3.45	1051,81	14,16	1048,36	
11					1038,0
T.P.	7,16	1043.32	15,65	1036,16	
10					1027,0
T.P	5.90	1032,91	16,31	1027,01	

May 2 1928 D. Parks, C. Rand, H. Clause

2.82	0,15	C2.7 / 23,0	1,81	C1.0 / 16.5
4.06	2.11	C1.9 / 21.5	6,04	F2.0 / 15.5
13,06	17,53	F0.5 / 18,5	11.87	C1.1 / 21.5
6,52	7,11	F0.6 / 19,5	5,39	C1.1 / 20.0
15,52	10.64	C4.9 / 27,5	6,06	C9.5 / 33,0
13,81	6,35	C7.5 / 29,0	1,64	C12.2 / 36,0
14,32	7,54	C6.8 / 27,0	2,51	C11.8 / 34,5

	+	1032,91	−		
9					1017.0
T.P.	1,05	1019,35	14.61	1018,30	
8					1005,00
T. P.	0,04	1004.19	15,20	1004,15	
7					993,00
T.P.	1,00	990,04	15,15	989,04	
6					981,00
T.P.	2.99	979,03	14,00	976,04	
B.M. Record.			5,98	973,05 973,04	

15,91 8,90 C7,0 / 24.5 4,00 C11,9 / 39,0

14,35 7,45 C6,9 / 29,0 3,38 C11,0 / 34,5

11,19 10,80 C0,4 / 15,0 14,54 F3,4 / 15,5

9,04 10,57 F1,5 / 17,0 12,37 F3,3 / 19,0

S.W. Co. N. H.W. Culvert 5+33

Chardon-Munson Town-Line Road. Slag No. 7

Initial	Number.	Weight.	
			Unloaded
			May 7
			May 8
B. & O.	330052		May 9

BM	5.65	1275.75		1270.10
T P	5.17	1279.55	1.37	1274.38
B M	4.29	79.73	4.11	1275.44
T P	4.14	1278.92	4.95	74.78
T P	3.25	1279.80	7.37	1271.55
B.M.			4.65	1270.15

Chardon Munson
Finished Grades

B.M.	0,29	1072,58		1072,29	
14					1066,0
T.P. 1	1,04	1062,19	11,43	1061,15	
13					1056,0
T.P. 1	1,41	1052,25	11,35	1050,84	
12					1042,0
T.P. 1	0,01	1040,94	11,31	1040,94	
11					1038,0
10					1029,0
T.P. 1	0,04	1028,57	12,41	1028,53	
9					1017,0
	0,63	1016,32	12,88	1015,69	
8					1006,0
			10,32		

B.M.	12,69	1084,98		1072,29	
T.P.	12,74	1096,40	1,34	1083,64	
	12,20	1108,51	0,09	1096,31	
20					1108,50
	10,64	1118,59	0,58	1107,93	
21					1114,25
	12,17	1130,73	0,03	1118,56	
22					1120,81

Fair Warm
Aug. 15, 1928 D. Parks, C. Rand, R. Hassel

60

Spike E. side of 20" stump

1066,0	2,58
1056,0	6,19
1042,0	6,25
1038,0	2,94
1029,0	11,94
1017,0	11,57
1006,0	11,32

Fair Warm
Aug. 21. 1928 D. Parks, C. Rand R. Hassel
Spike E. side of 20" Stump.

1108,50	0,01
1114,25	4,31
1120,81	9,92

		1130.73		
23				1129,00
	12.78	1143,34	0,17	1130,56
24				1138,00
	12,20	1155,38	0,16	1143,18
25				1147,00
24				1153,00
	7,47	1162,52	0,33	1155,05
27				1158,25
27/60				1153,80
	2,97	1158,97		1153,80
26				1153,44
25				1147.00
	0,34	1144,08	12,88	1143,74
24				1138,00
	0,35	1141,69	12,74	1131,34
23				1129,00
22				1120,81
	0,44	1114,58	12,55	1119,14
21				1114,25
20				1108,50
	1,55	1114,97	6,16	1113,42
	0,21	1102,49	12,69	1102,28
	1,51	1092,49	11.01	1091,48
B.M.	1,29	1081,46	12,82	1080,17
			8,38	1072,08

1,73	
5,34	
8,38	
2,38	
4,27	
3,52	

Left slope hub sta 26

2,97	
8,97	
6.08	
2,29	
10,87	
6,33	
16,08	
	1072,17 record

Initial.	No. / Number.	SLAG Weight	Unloaded	From Sta.	To Sta.
B.&L.E.	42978				

	2,97	1155,97		1153,00	
26					1153,00
25					1147,00
	0,84	1144,08	12,23	1143,74	
24					1138,00
	0,85	1131,69	12,74	1131,34	
23					1129,00
22					1120,81
	0,44	1119,58	12,55	1119,14	
21					1114,25
20					1108,50
	1,55	1117,97	6,16	1113.42	
	0,81	1102,49	12,69	1102,28	
	1,51	1092,99	11,01	1091.48	
	1,29	1081,76	12,82	1080,17	
B.M			8,38	1072,08	
				1072,27	record

Left Slope Hub Sta 26.

2,97

8,97

4,08

2,69

10,88

5,33

11,08

Spike in E. side of 20" stump

B.M.	3.97	1076.76		1072.29	
14					1065.0
15					1074.0
	12.30	1087.93	0.23	1075.63	
16					1082.0
	10.18	1097.97	0.14	1087.79	
17					1089.5
18					1097.0
	10.53	1107.55	0.95	1097.02	
19					1102.75
	7.21	1114.07	0.69	1106.86	
20					1108.50
B.M	0.59	1078.88		1072.29	
	1.11	1063.82	10.17	1062.71	
13					1056.0
	0.47	1051.23	13.06	1050.76	
12					1047.0
	0.65	1040.05	11.83	1039.40	
11					1038.0
10					1029.0
	0.56	1027.60	13.01	1027.04	

Cloudy Windy
Aug. 30, 1928 D. Parks, C. Rand, R. Hassel
Spike in E side 20" Stump.

11.26	11.6
2.26	2.8
5.93	6.8
8.47	9.3
0.97	1.7
4.80	5.5
5.57	

Cloudy Windy
Aug. 31, 1928. D. Parks, C. Rand
Spike E side 20" Stump

7.82	
4.23	4.7
2.05	2.4
11.05	11.4

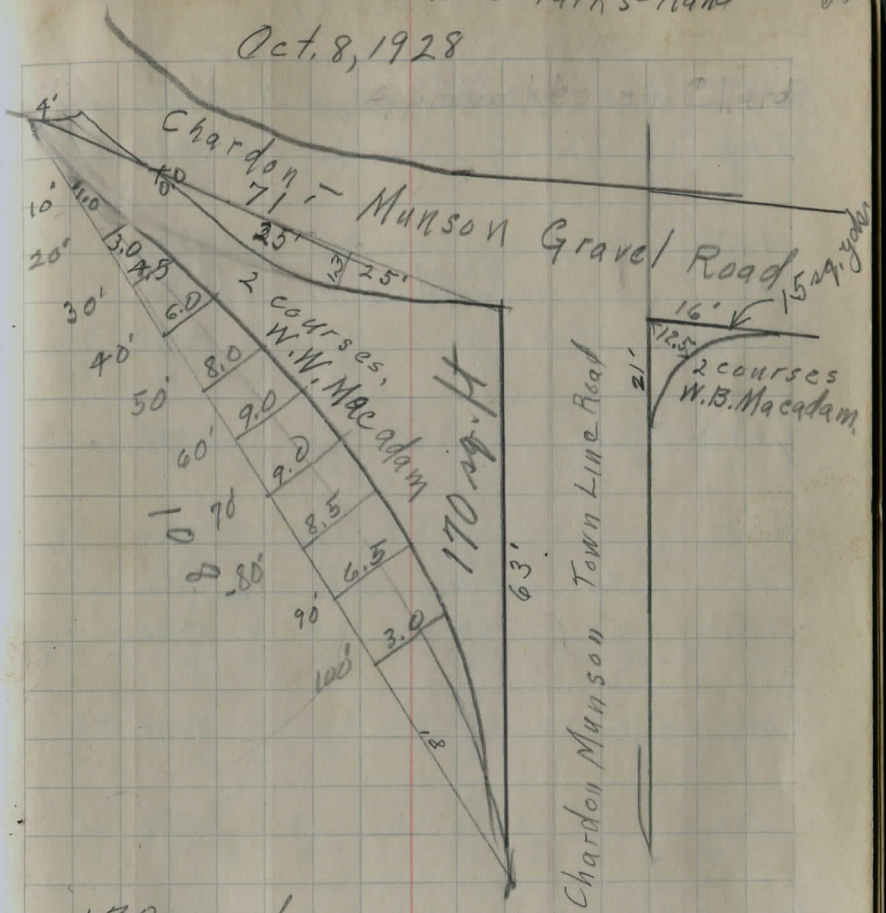
		1027,60			
9					1017,0
	0,14	1015,38	12,46	1015,14	
8					1006,0
	0,05	1003,17	12,18	1003,12	
7					
	0,40	990,59	12,98	990,19	
6					
	0,75	978,35	12,99	977,60	
5					
4					
	0,43	965,83	12,95	965,40	
3					
2					
	1,80	955,27	12,36	953,47	
1					
0					
T.P.			9,83	945,44	

Sub. Grade

Rod	Elev.
10,60	11,00
10,3	10,7. 1005,10
8,8	994,37
6,4	984,19
3,7	974,45
11,6	966,75
5,9	959,93
11,4	954,43
4,6	950,67
9,1	946,17

Hub Rt Stg 0+00

Oct. 8, 1928



170 sq. yds.
15 sq. yds.
185 sq. yds., both approaches.

Bass Lake Rd

Continued from Pg 25

BM #6	4.79	44.42 / ~~38.41~~		9.63 ✓ Elev. corrected / 123~~7.62~~
39+0				36.72
+50				32.92
T.P. 15	0.15	32.94 / ~~26.93~~	11.63	32.79 / 12~~6.78~~
40+0				29.24
+50				25.94
41+0				23.54
TP 16	3.79	26.32 / ~~20.31~~	10.41	22.53 / 12~~6.52~~
+50				22.32
42+0				21.42
+50 ✓				20.52
43+0				19.82
TP 17	2.09	21.15 / ~~15.14~~	7.26	19.06 / 12~~3.05~~
44+0				18.85
45+0				17.85
46+0				16.75

W E

Hortg. Spk Rd face CEI

5.3/30		6.5/16	8.4/12	7.7/2	7.7	8.0/8	7.6/10	4.5/18	4.1/30
9.4/30		10.9/17	12.0/11	11.4/3	11.5	12.7/8	11.4/12		7.8/30
2.2/30		3.7/16	5.3/13	4.5/12	3.7	4.7/11	3.8/15		0.65/30
7.0/30	6.8/22	7.7/17	8.7/13	7.7/10	7.0	7.7/10	8.9/15	7.9/20	7.0/23	7.0/30
9.8/30		10.0/18	11.3/14	10.2/10	9.4	10.0/11	10.6/16	10.0/19	10.6/30
5.3/30	4.9/19	5.5/17	6.1/13	4.8/10	4.0	4.0/2	4.7/13	5.5/16	4.9/18	4.5/30
	7.7/30		7.8/18	7.5/12	5.7/9	4.9	4.9/2	5.3/12	6.8/16	6.3/18	5.9/30
	7.6/30	7.7/16	8.6/12	6.6/9		5.8	5.8/2	6.0/12	7.3/15	6.0/30	
	8.0/30	8.0/18	8.9/12	7.3/9		6.5	6.5/2	7.3/13	6.3/16	7.0/21	6.5/30
	3.2/30	3.3/16	4.6/13	3.2/9		2.3	2.2/2	2.8/13	4.0/16	3.0/19	2.7/30	
	3.9/30	3.9/13	5.6/11	4.2/9		3.3	3.2/4	4.2/15	5.2/17	4.1/19	3.2/30	
	4.3/30	4.8/15	6.6/12	5.3/9		4.4	4.3/3	5.6/14	6.4/16	5.0/20	4.1/30	

		21.15 12 ~~15.14~~			
47+0				15.45	
48+0				14.15	
49+0				13.35	
B.M. #7			5.83	15.32 12 ~~09.31~~	Elev Corrected
T.P. 15	2.45	15.29 12 ~~09.28~~	8.31	12.84 12 ~~06.83~~	
50+0				12.29	
51+0				11.79	
52+0				10.89	
53+0	Retaining wall needed			10.39	
54+0				09.79	
55+0				8.59	
56+0				7.89	
T P 19	4.89	12.32 12 ~~06.81~~	7.36	07.93 12 ~~01.92~~	
57+0				7.82	
58+0				7.52	

W E

6.2/30	6.0/15	7.7/12	6.6/10	5.7	5.7/3	6.4/13	7.6/15	6.9/20	5.6/30
6.5/30	7.1/16	7.6/15	8.7/11	8.0/9	7.0	7.0/3	7.9/15	8.8/17	7.5/20	8.0/30
7.9/40	8.8/15	9.8/11	8.5/9	7.8	7.8/3	8.6/11	11.1/17	9.8/22	9.0/30

Heat 5PR Twin Cherry Sta 48+40 30' Rt ℄

2.5/30	4.3/20	4.7/14	4.0/11	3.0	3.0/3	3.8/12	3.5/14	6.6/18	7.1/21	3.4/23	3.4/30
4.4/30	4.3/17	5.3/15	4.3/10	3.5	3.6/3	4.3/15	4.6/18	7.9/22	7.5/26	5.0/28	4.0/30
5.0/30	5.0/17	6.1/12	5.2/10	4.3	4.3/2	5.2/14	7.7/16	7.5/20	5.3/24	4.7/30	
4.6/30	3.7/20	5.9/14	6.6/12	5.7/10	4.9	4.9/1.5	5.5/11	8.1/15	8.1/21	5.3/24	4.6/30
5.2/30	6.4/15	7.5/12	6.3/9	5.5	5.4/2	6.3/14	8.5/16	9.0/24	6.0/26	5.9/30	
6.1/30	6.4/17	7.1/16	8.7/14	8.0/10	6.7	6.7/3	7.6/14	9.6/18	10.2/24	7.2/26	6.8/30
7.1/30	6.7/20	9.1/12	8.7/10	7.4	7.3/4	8.7/16	11.3/20	11.2/26	8.0/30		
5.8/30	6.7/17	7.0/19	6.1/10	5.0	4.9/3	5.8/14	6.5/17	8.8/20	8.8/26	6.6/28	out
6.4/30	6.6/20	7.1/17	7.3/12	6.5/9	5.3	5.2/3	6.0/15	9.2/17	9.2/25	6.2/30	

		12.82 / 120~~6.61~~			
59+0				7.62	
BM * 8	6.07	15.19 / 120~~9.18~~	3.70	9.12 / 120~~3.11~~	✓ Elev Corrected
60+0				8.39	
61+0				9.29	
62+0				9.19	
TP 20	6.02	14.67 / 120~~8.66~~	6.54	8.65 / 120~~2.64~~	
63+0				8.67	
64+0				8.57	
65+0				8.87	
66+0				9.57	
67+0				10.47	
68+0				11.97	
TP 21	10.78	25.15 / 12~~19.14~~	0.30	14.37 / 120~~8.36~~	
69+0				14.15	
70+0				17.35	

W E

6.7/30 6.7/18 7.8/13 D 6.9/11 5.9/7 ○ 5.2 □ 5.1/4 5.7/14 7.9/17 9.6/20 D 9.3/24 6.2/30

NET E Hdwl. Sta 59+90

7.4/30 8.5/19 10.6/15 7.7/9 6.9/6 ○ 6.8 □ 6.9/4 6.8/12 9.2/16 11.6/20 10.5/30

59+90 Culvt 11.9/11 11.6/7 OL 6.8 11.5/14 EL

5.4 Drive ○ 5.9 □ 6.0/4 7.0/16 8.5/19 7.5/22 7.6/30

5.9/30 6.7/13 D 7.9/10 7.0/8 ○ 6.0 □ 5.9/5 6.8/15 D 7.6/17 8.2/20 6.9/26 5.9/30

5.9/30 7.3/19 D 7.7/11 6.8/9 ○ 6.0 □ 6.0/4 7.2/16 D 7.8/18 7.1/20 7.3/30

6.3/30 7.2/12 ○ 7.9/10 7.2/8 ○ 6.1 □ 6.1/4 6.9/15 D 7.5/18 7.1/21 7.8/30

7.8/30 7.3/13 D 7.5/11 6.5/9 ○ 5.8 □ 5.7/3.5 6.2/17 Drive 7.2/30

6.6/30 D 6.5/11 5.9/10 ○ 5.1 □ 5.0/3 5.9/15 D 6.5/17 5.5/20 6.8/30

5.5/30 5.1/13 D 5.5/11 4.9/9 ○ 4.2 □ 4.2/2 4.9/15 D 5.9/18 4.5/20 5.0/30

3.7/30 3.4/21 3.6/13 D 9.1/12 3.3/10 ○ 2.7 □ 2.6/1 3.3/14 D 4.5/19 1.8/30

9.4/30 9.9/19 11.9/13 D 12.5/12 12.0/10 ○ 11.0 □ 11.0/2 11.7/15 D 13.6/18 11.6/19 8.8/30

7.4/30 7.2/17 9.6/13 8.8/11 ○ 7.8 8.0/11 Drive 6.8/30

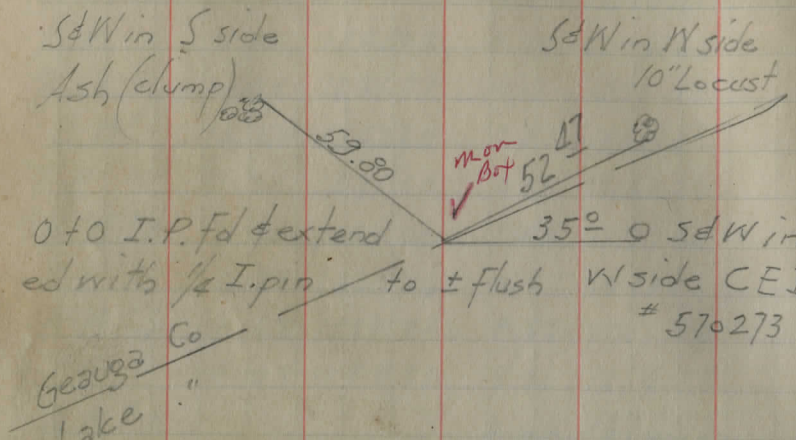
		AL 25.15 1219.14		
71+0				19.95
72+0				22.25
TP 22	10.68	35.34 1229.33	0.49	24.66 1218.65
73+0				24.54
74+0				26.84
75+0				28.44
76+0				29.94
77+0				31.84
+69			0.45	1234.89
TP 23	0.43	1220.93	8.75	1220.58
T.P. 24	0.06	1210.52	10.47	1210.46
TP 25	5.76	1207.14	9.14	1201.38
B.M. #8			4.17	1202.97
B.M. #8	4.17	1207.28	0.70	1203.11
TP 26	8.53	1209.41	6.40	1200.88
TP 27	7.53	1214.72	2.22	1207.19
B.M. #7			5.41	1209.31
T.P. 28	10.96	1224.18	1.50	1213.22
	11.73	1232.77	3.14	1221.04

5.2/30	4.9/16	D 6.9/13	6.1/11	D 5.2	5.6/13	D 7.0/15	3.5/23	3.4/30
2.4/30	2.1/17	D 4.5/12	4.1/11	D 2.9	3.8/13	D 4.9/17	1.6/23	1.1/30
10.7/30	10.2/17	12.2/12	12.0/11	D 10.8	11.3/13	D 13.0/17	8.2/30	
9.6/30	8.7/17	10.3/14	9.6/12	D 8.5	9.2/13	D 10.8/15	6.6/23	6.0/30
9.3/30	7.9/17	D 8.3/14	7.9/13	D 6.9	7.3/13	D 7.8/15	6.2/23	5.8/30
7.6/30	6.1/18	D 6.6/15	6.0/13	D 5.4	5.9/12	D 6.9/15	5.10/18	6.0/30
1.3/30	1.8/17	4.7/13	4.3/11	3.5 3.5/2	4.4/16	5.1/17	3.3/22	1.6/30

0.45 Pavement edge

		1232.77		
T P 29	8.49	1238.92	2.34	1230.43
B.M. #6			5.31	1233.61
T. P. 30	11.35	1245.98	4.29	1234.63
T. P. 31	10.98	1256.81	0.15	1245.83
B.M. #5	10.17	1263.60	3.38	1253.43
T.P. 32	11.90	1275.10	0.40	1263.20
B.M. #4	6.35	1280.00	1.45	1273.65
T P 33	6.23	1285.36	0.87	1279.13
B M #3	0.68	1283.44	2.60	1282.76
T.P. 34	4.09	1279.37	8.16	1275.28
B M #2			2.62	1276.75
B M #3	0.63	1283.39		1282.76
T P 35	2.37	1279.27	6.49	1276.90
B M #2	2.72	1279.37	2.62	1276.65
T.P. 36	0.11	1276.82	2.66	1276.71
T.P. 37	5.13	1273.50	8.45	1268.37
B M #1			3.93	1269.57

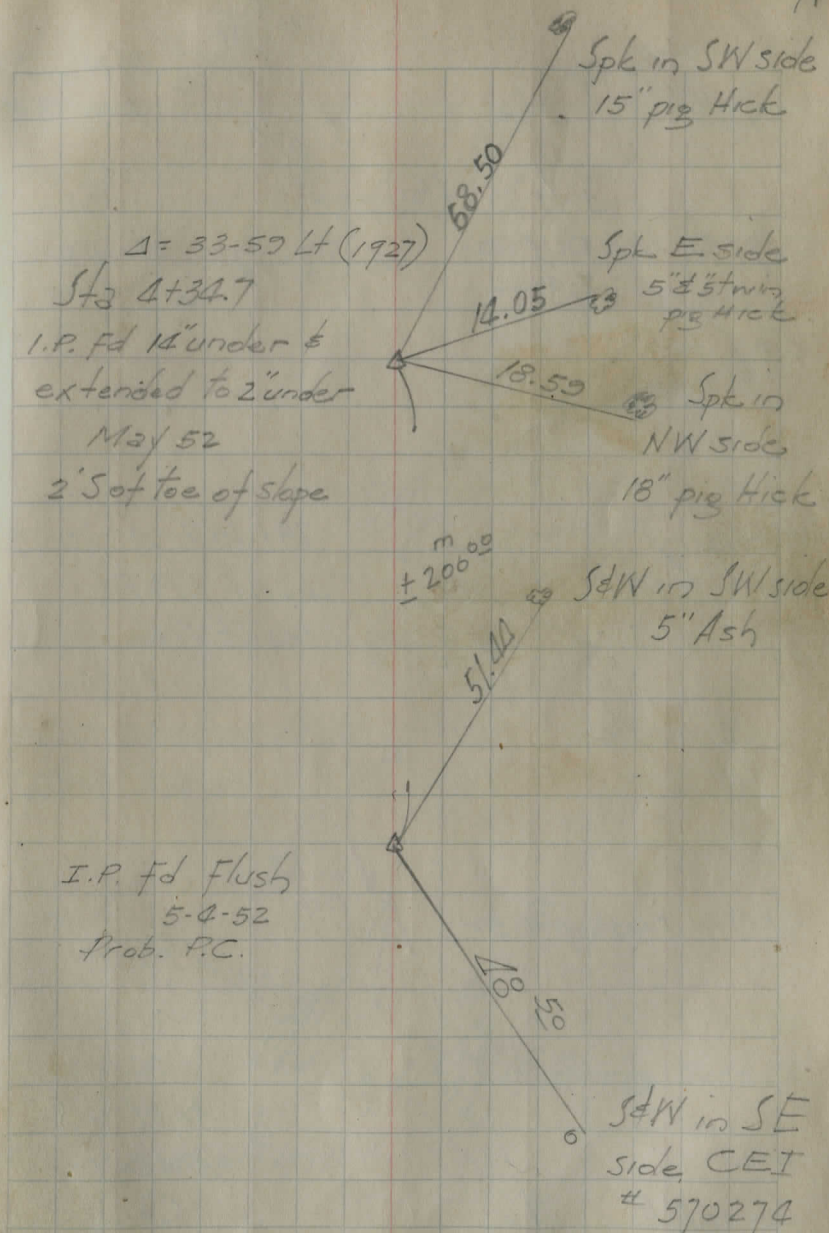
75.14
69.57
5.87

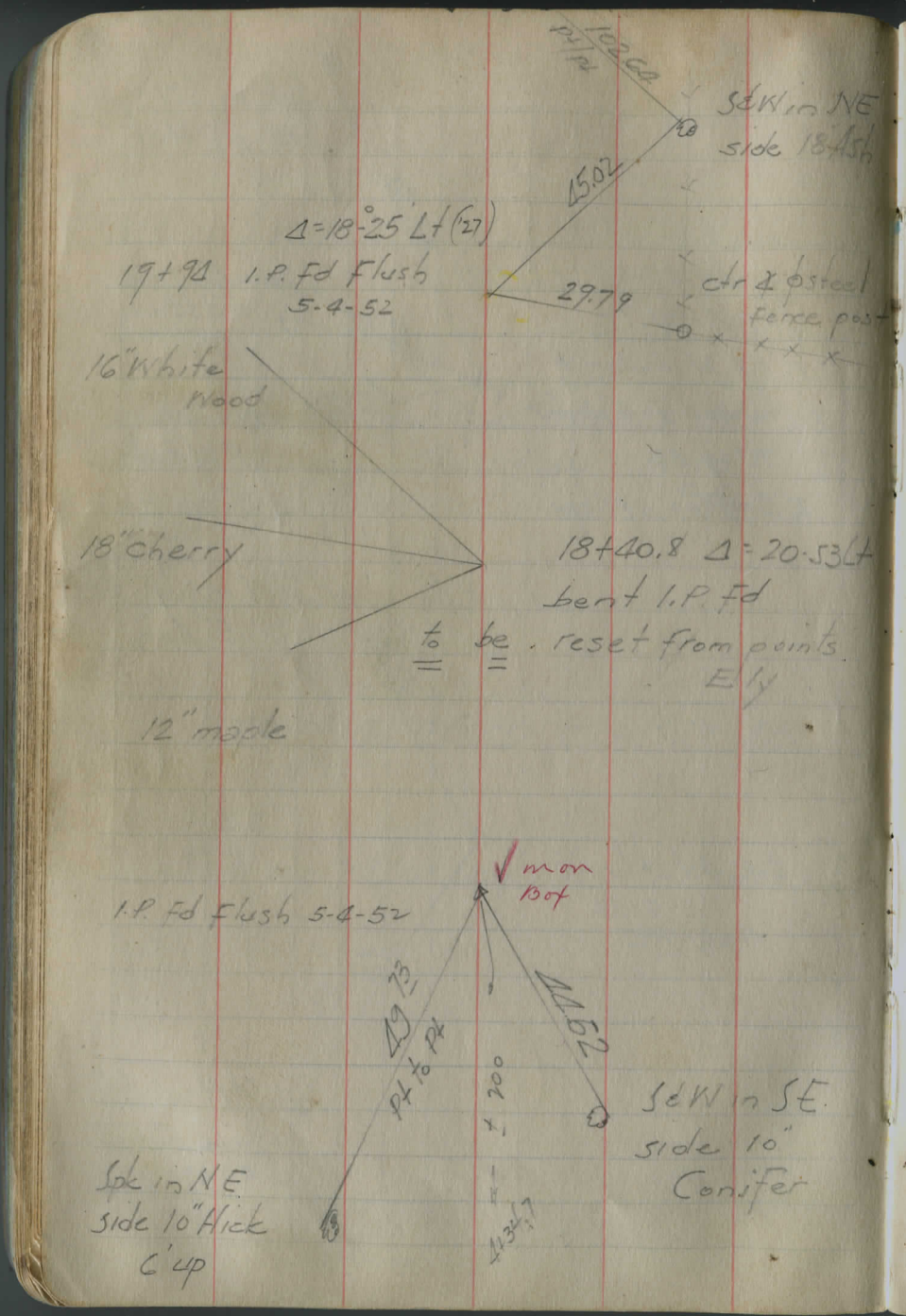


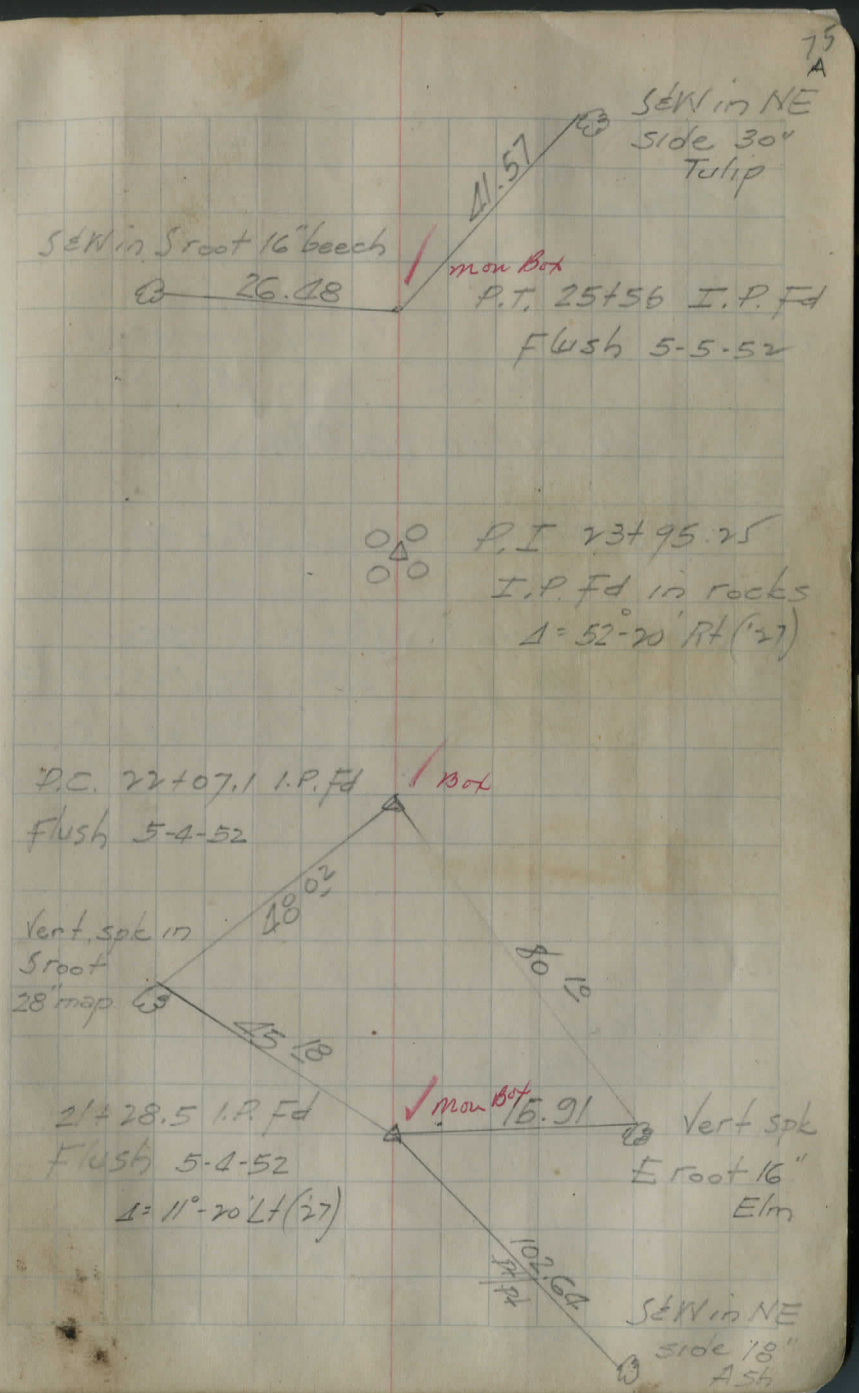
THWING ROAD C.H. #27 ABC

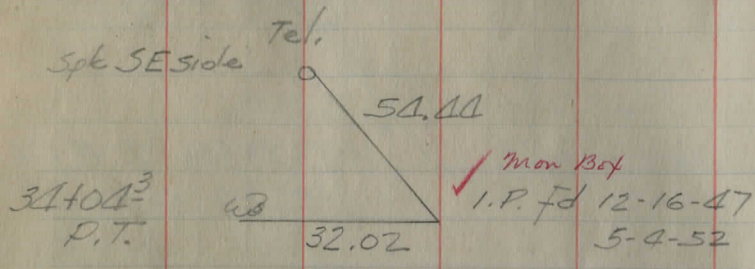
5-3-52

See pg 78 et seq For 1927 notes



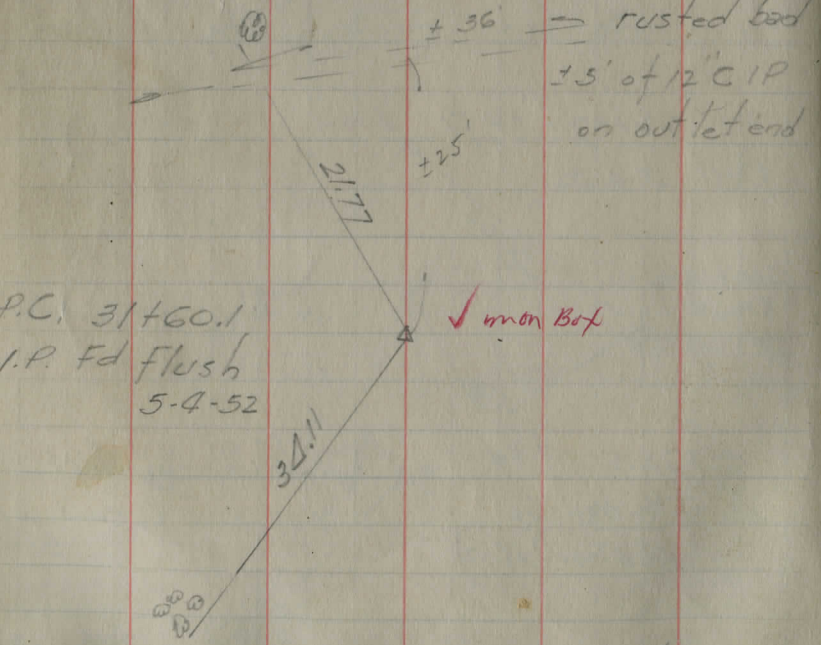

102.64 Pt to Pt
S&W in NE side 18" Ash
45.02
Δ=18°-25' Lt (27)
19+91 I.P. Fd Flush 5-4-52
29.79
ctr & post steel fence post
16" White wood
18" Cherry
18+40.8 Δ=20-53 Lt
bent I.P. Fd
to be reset from points
E ly
12" maple
mon Bot
I.P. Fd Flush 5-4-52
49.73
Pt to Pt
41.52
± 200
41+34.7
S&W in SE side 10" Conifer
Spk in NE side 10" Hick
C'up

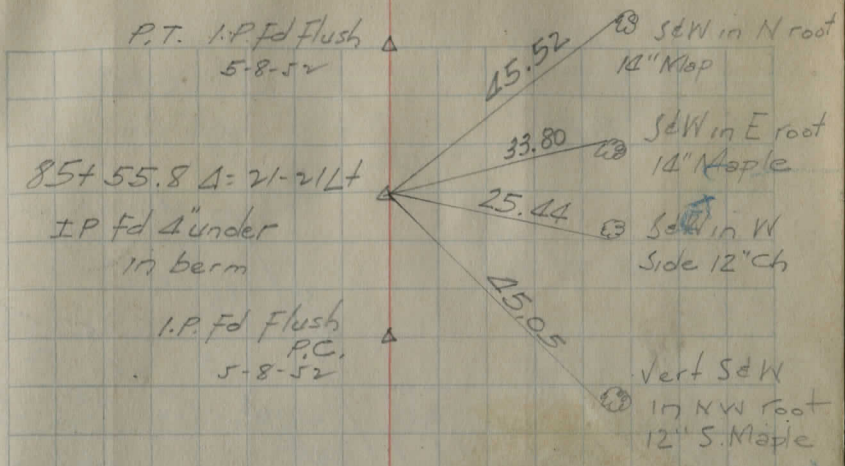

S&W in NE side 30" Tulip
41.57
S&W in S root 16" beech
mon Bot
26.08
P.T. 25+56 I.P. Fd Flush 5-5-52
P.I 23+95.25
I.P. Fd in rocks
Δ=52°-20' Rt (27)
P.C. 22+07.1 I.P. Fd Flush 5-4-52
Bot
Vert. spk in S root 28" map
18° 02'
80 10
45.18
21+28.5 I.P. Fd Flush 5-4-52
Δ=11°-20' Lt (27)
mon Bot
15.91
Vert spk E root 16" Elm
102.64 Pt to Pt
S&W in NE side 18" Ash

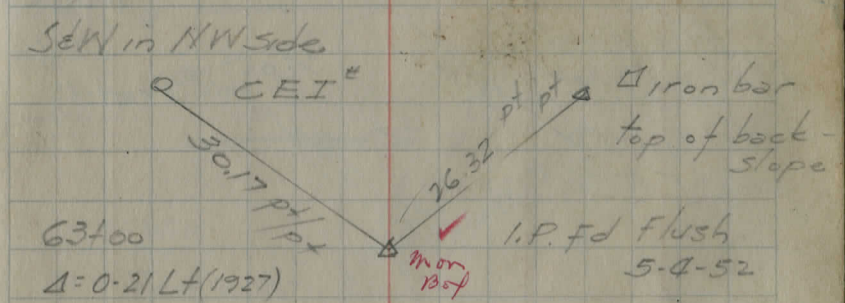


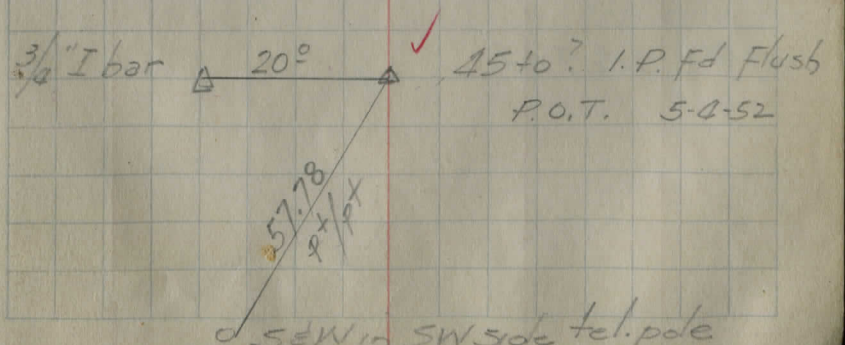
Spk W side 26" Map.

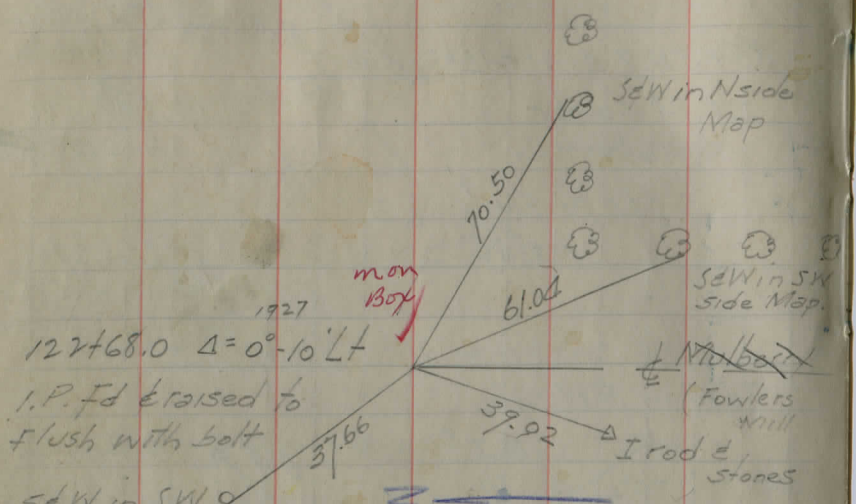
31+82.5 Δ = 9-36 Et (1927) no look for 1952











12+68.0 Δ = 0°-10' Lt

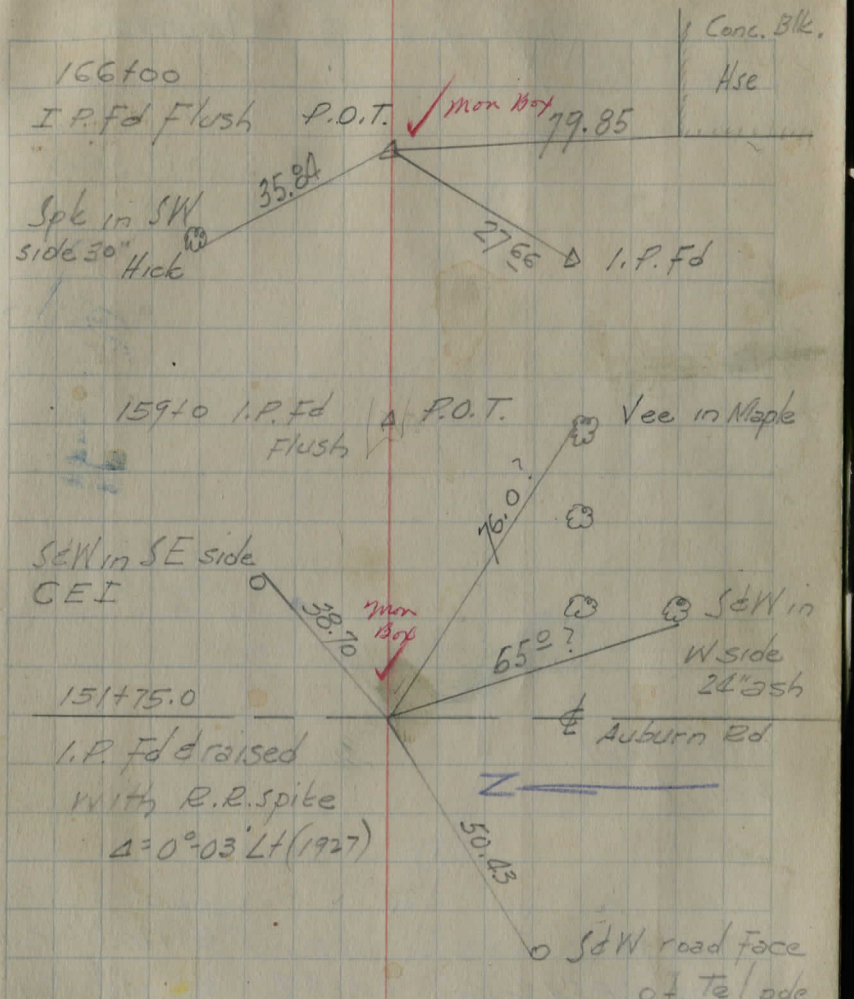
I.P. Fd & raised to flush with bolt

14.3 x 8" plank broken

18' overall span

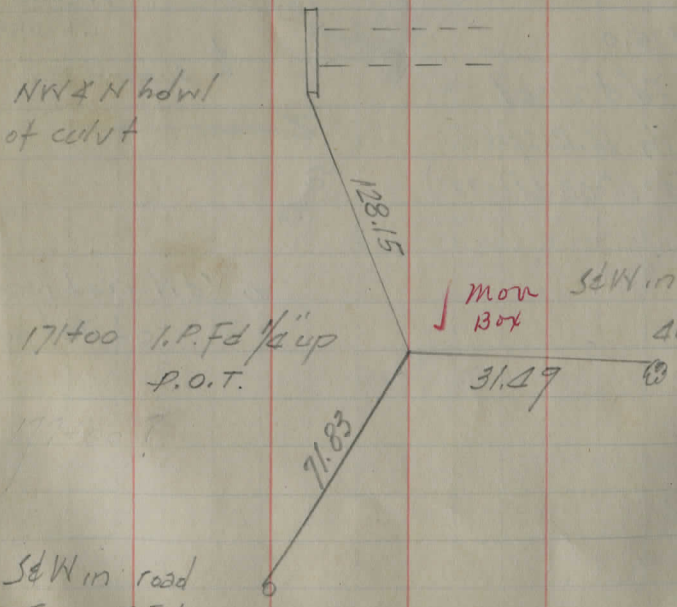
16' between posts

119+70 No Find

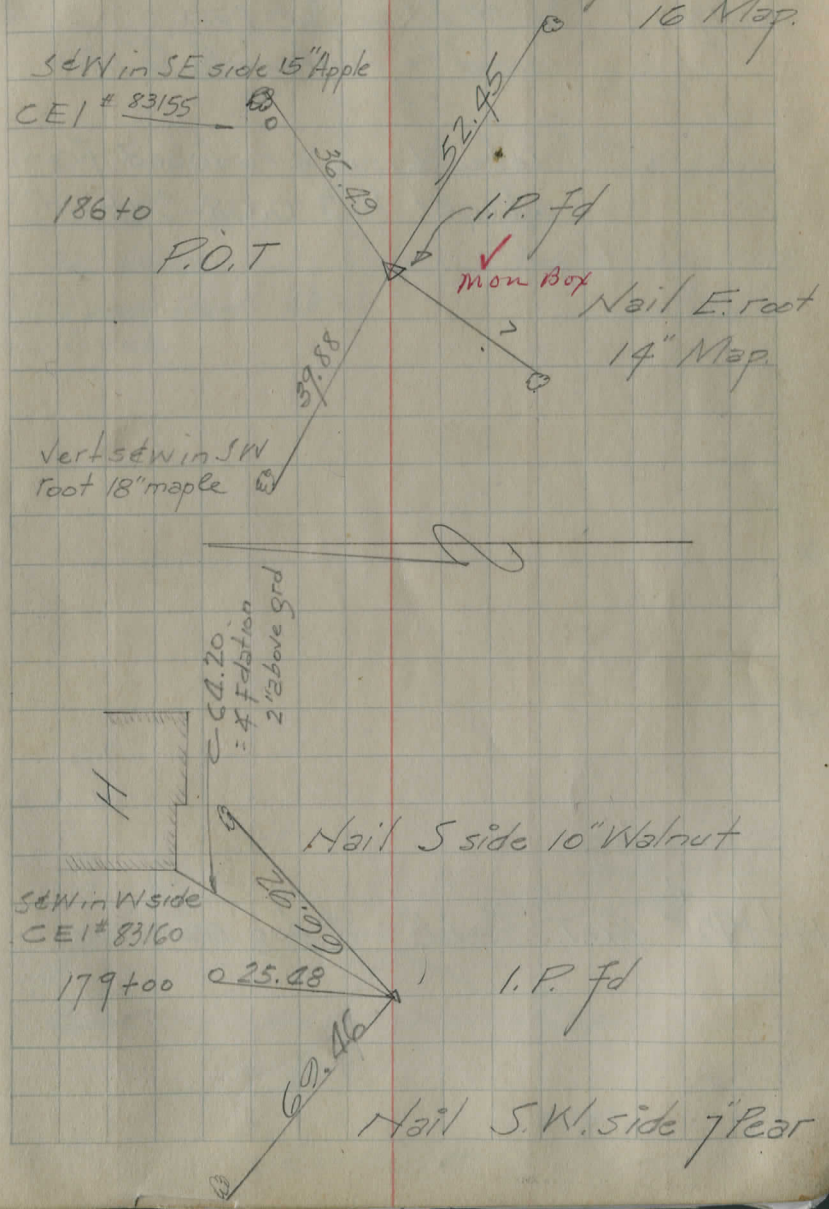


5-12-42
Pom - Gund.
5-9-52
Pom - Maynard

Ref for ℄ Munson



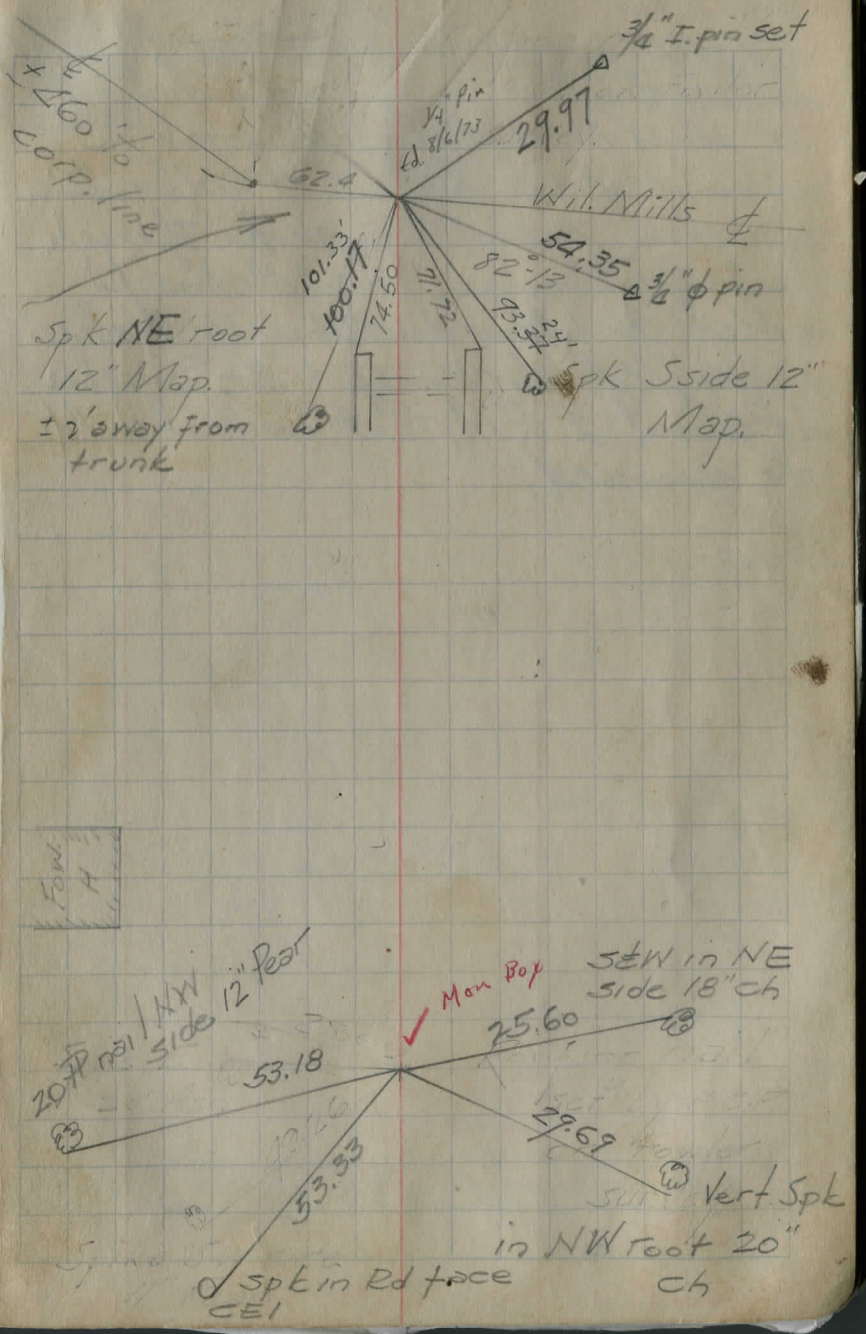
Chardon Twp Line



203+71.7 ½" I.P. fd under pavt raised to Flush with ⅛" I.P. 5-15-52

Note: Line produced From West hits 0.08 S of I.P.

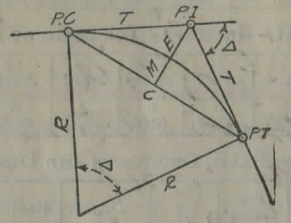
194+90 ± P.O.T. I.P. set Aug '52



May 11. Chardon-Munson Town Line Road
Sub-Contractor Knapp received orders
at about 10 A.M. to stop work, on
account of his disregard to direction
given him by Asst. Engr. Marks through
Inspector Douglas, After Mr. Knapp
agreed to follow directions, Mr. Marks
instructed Mr. Knapp & Mr. Douglas
at about 2 P.M. that work should
be resumed.

19

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7) =R÷cos. $\frac{\Delta}{2}$ −R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161 +60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C. +L=164 +91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′÷2=6° 26.2′, etc.

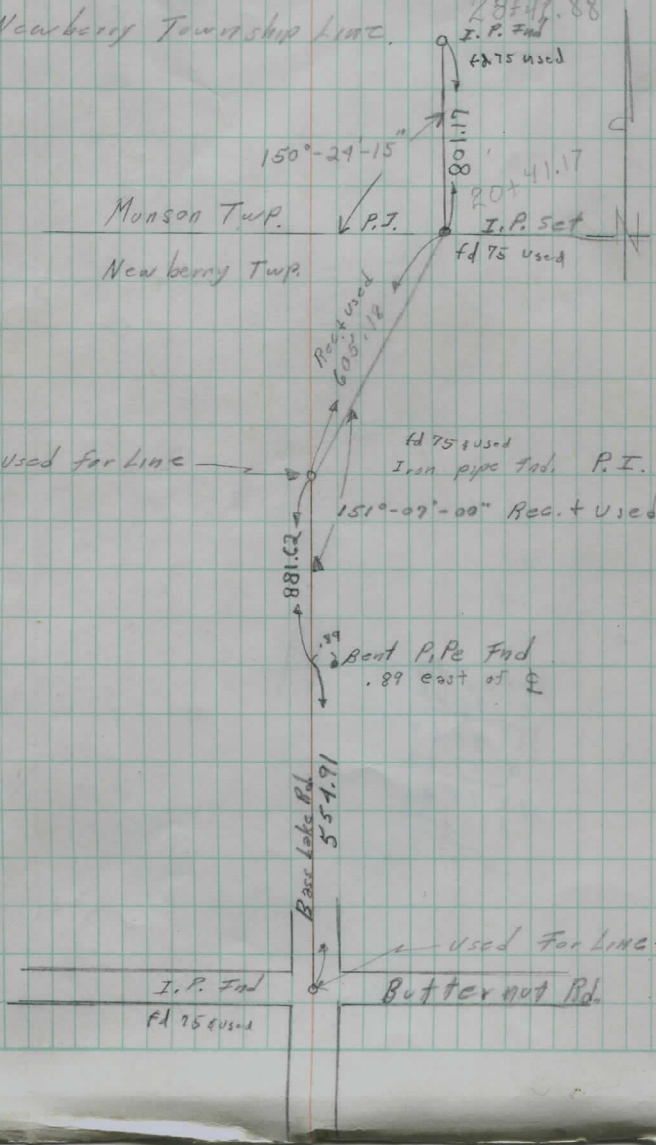
Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.

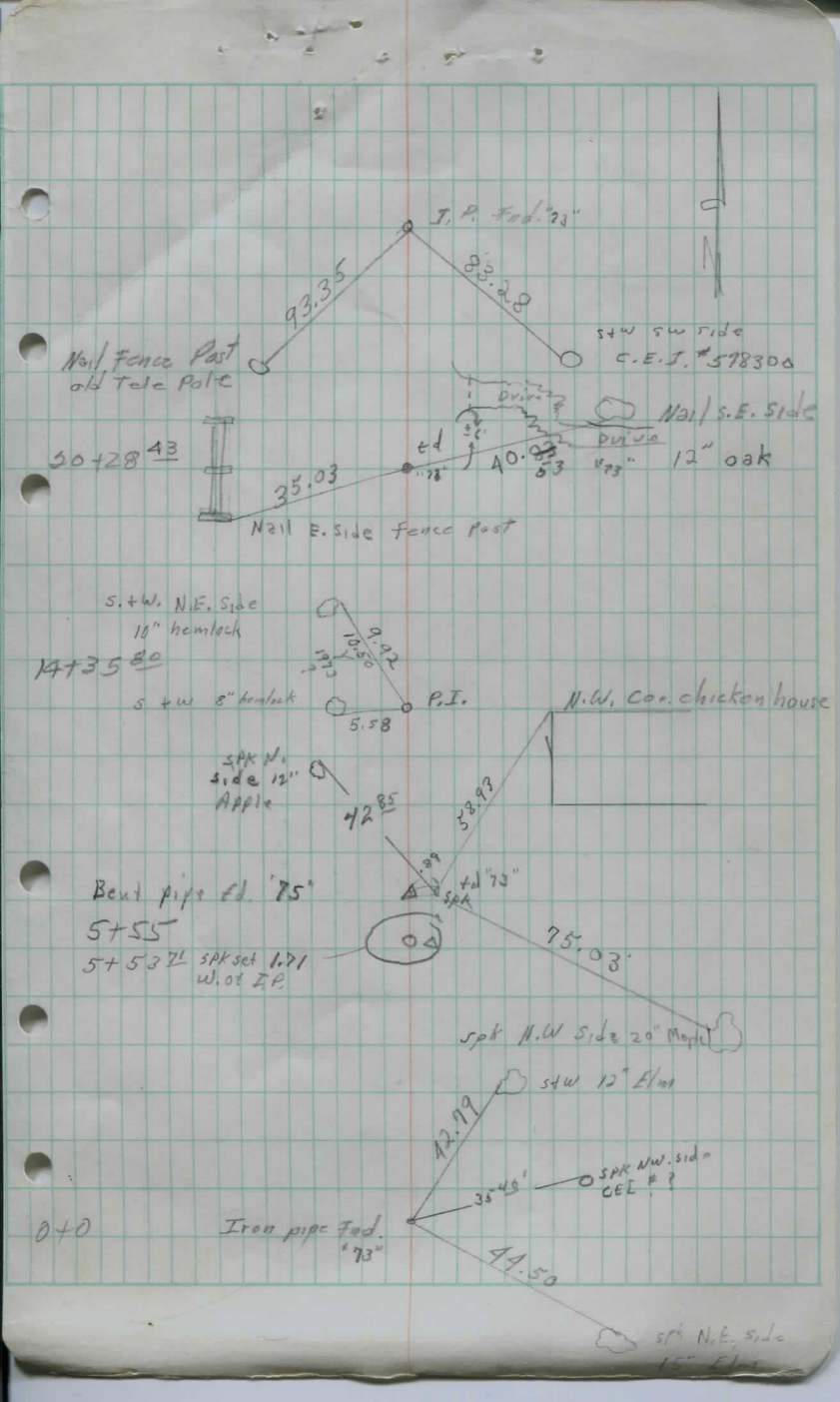
Bob Kosie
Don Kosie
Paul Rooney

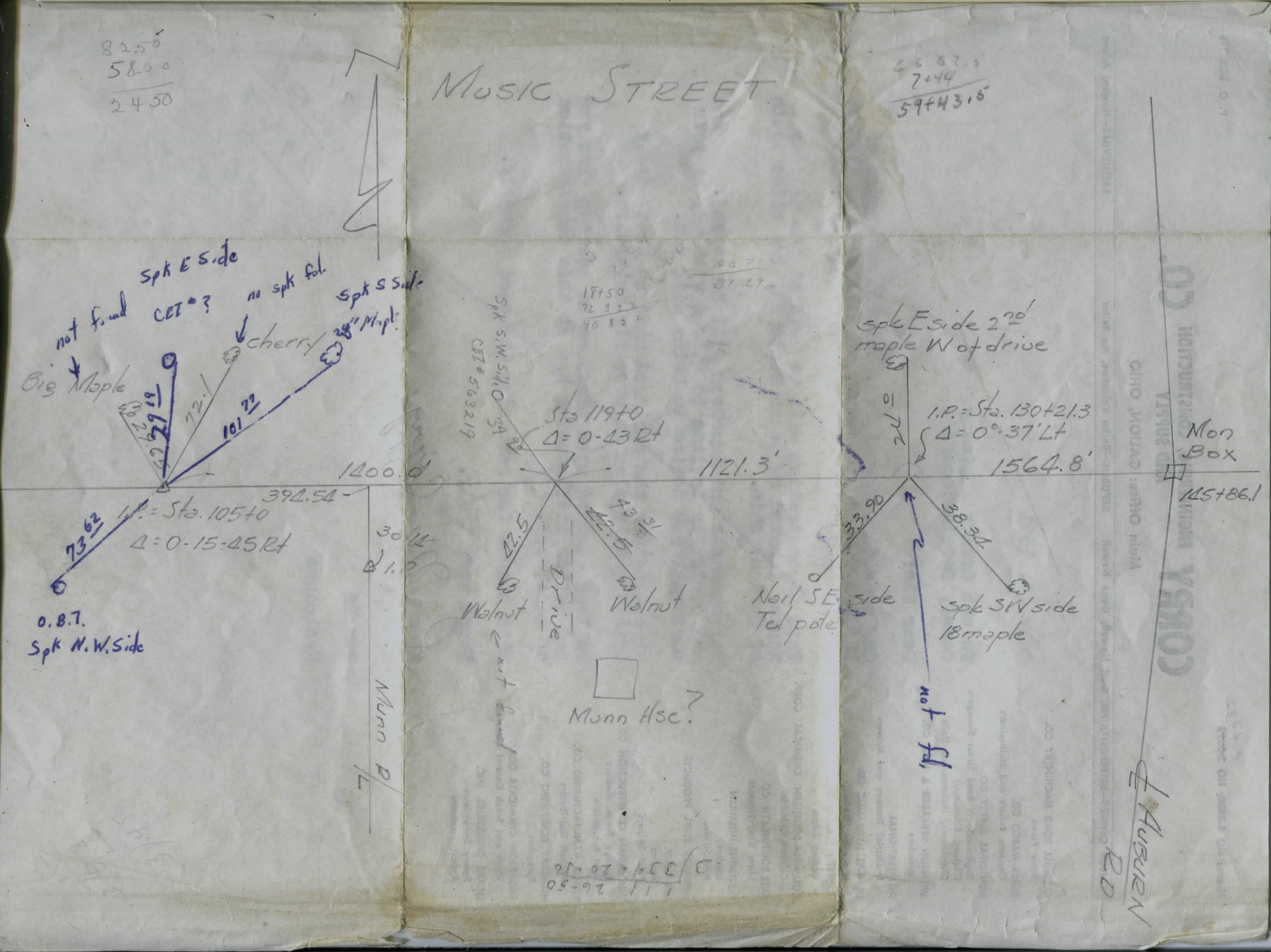
12/20/69

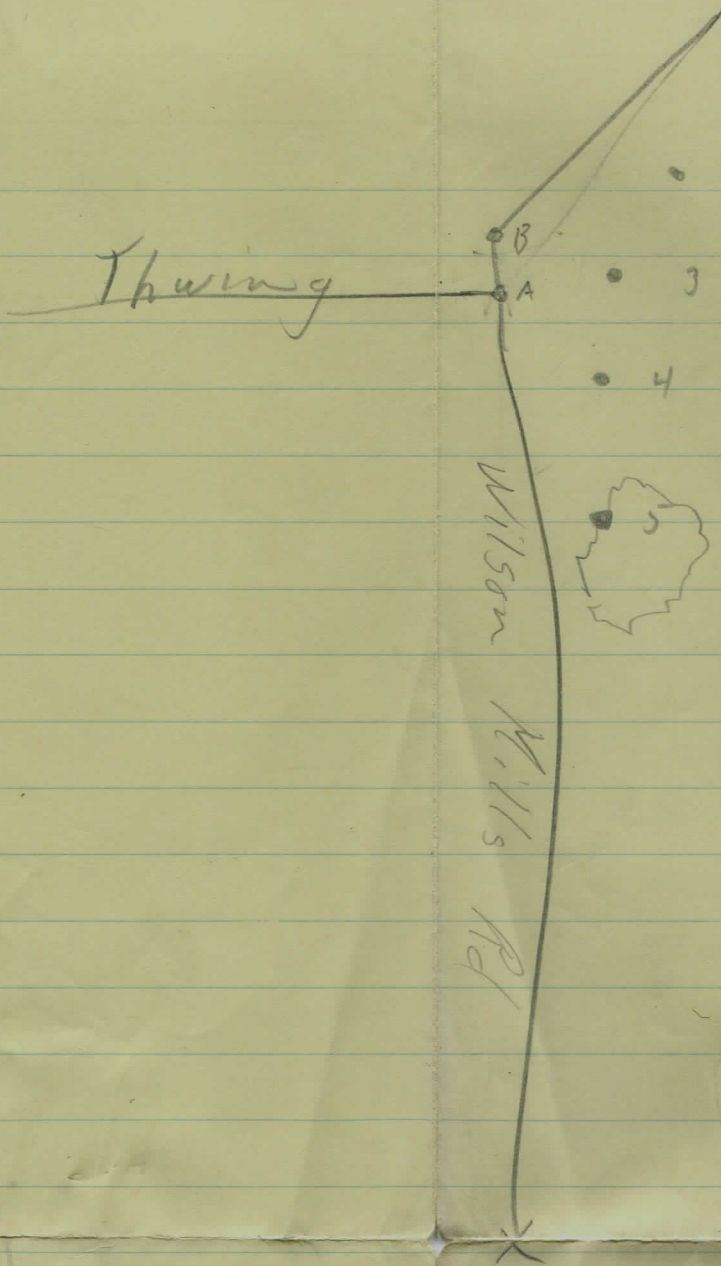
& Info. Bass Lake Rd North to Munson
Newberry Township Line.

28+45.88



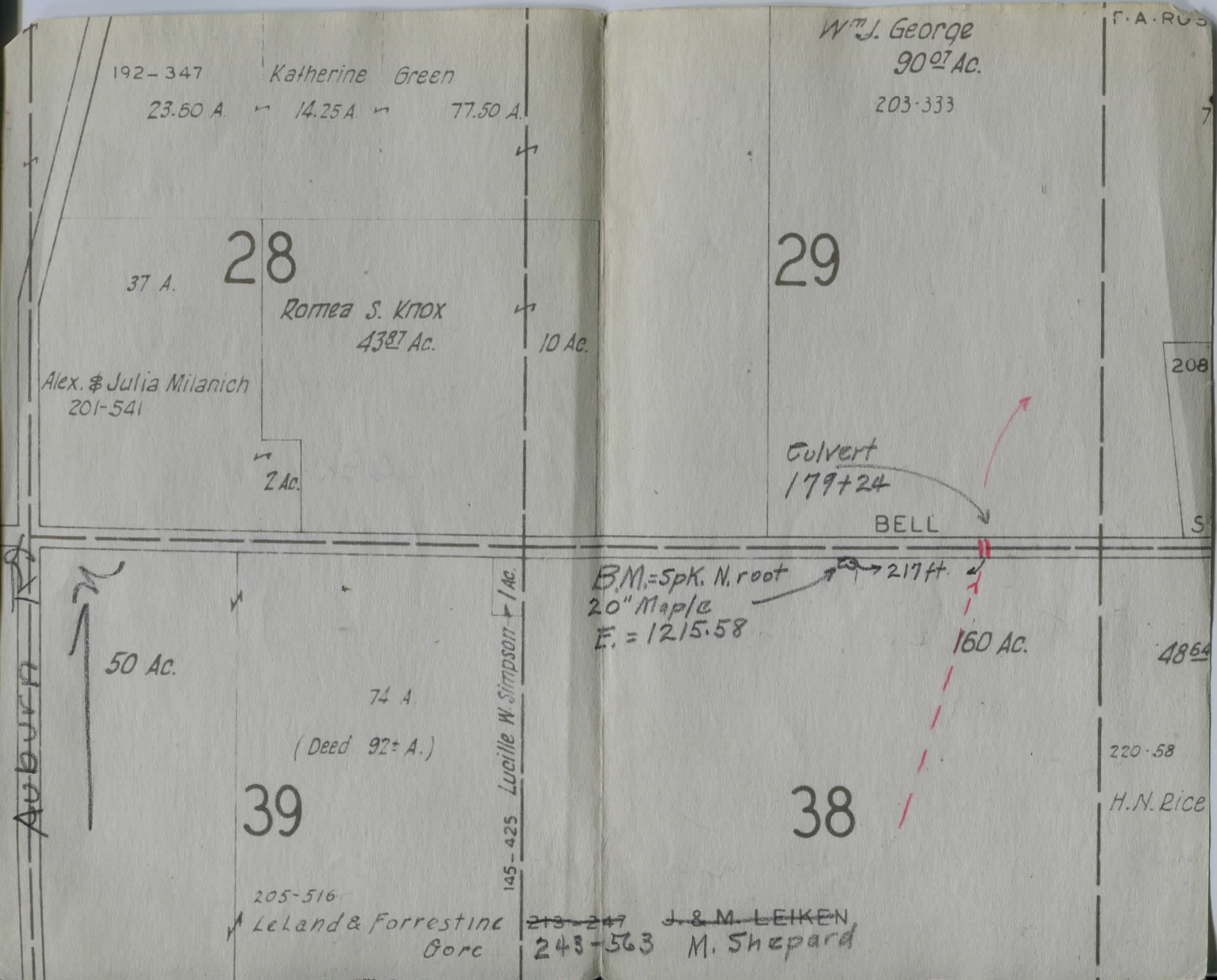

I. P. Fnd. "73"
93.35
83.28
Nail Fence Post
old Tele Pole
S+W SW side
C.E.I. # 57830
Drive
Drive
Nail S.E. Side
12" oak
50+28 43
35.03
Nail E. Side Fence Post
40.53
Fd "73"
S. + W. N.E. Side
10" hemlock
14+35 80
S + W 8" hemlock
9.42
P.I.
5.58
N.W. Cor. chicken house
Spk N. side 12" Apple
42 85
38.93
Bent pipe Fd. '85"
5+55
5+53 71 Spk set 1.71 W. of P.I.
Spk Fd "73"
75.03
Spk N.W Side 20" Maple
S+W 12" Elm
42.79
35 45
Spk NW. side CEL # ?
0+0
Iron pipe Fnd. "73"
44.50
Spk N.E. Side 15" Elm


MUSIC STREET
825.0
58.00
2450
Spk E Side
not found
CET#?
no spk fd.
Spk S Side
cherry
Big Maple
29.19
72.1
101.72
1200.0'
394.54
I.P. = Sta. 105+0
Δ = 0-15-45 Rt
73.62
30.14
O.B.T.
Spk N.W. Side
Munn P/L
Spk S.W. side 10" cherry
CET# 563219
Sta 119+0
Δ = 0-43 Rt
1121.3'
42.5
43.31
42.5
Drive
Walnut
Walnut
Munn Hse?
Spk E side 2nd maple W of drive
I.P. = Sta. 130+21.3
Δ = 0°-37'Lt
1564.8'
Mon Box
145+86.1
33.90
38.34
Nail SE side Tel pole
Spk SW side 18 maple
not fd.
Auburn
20



Set on A - Sight on B. Clockwise ∠

CEI #		Hor. ∠	Sta Dist.
#46415	①	33°-31'	243.0'
" 46417	②	30°-54'	100.0'
No No	③	73°-58'	25.0'
46415	④	170°-10'	142.0'
46414	⑤	175°-05'	290.0'


192-347
Katherine Green
23.60 A.
14.25 A.
77.50 A.
28
37 A.
Romea S. Knox
43.87 Ac.
10 Ac.
Alex. & Julia Milanich
201-541
2 Ac.
Wm J. George
90.07 Ac.
203-333
29
Culvert
179+24
BELL
208
B.M.=Spk. N. root
20" Maple
E. = 1215.58
217 ft.
160 Ac.
50 Ac.
74 A.
(Deed 92± A.)
Auburn Rd.
Lucille W. Simpson
1 Ac.
145-425
39
205-516
Leland & Forrestine Gore
213-247
J. & M. LEIKEN
243-563
M. Shepard
38
220-58
H.N. Rice

370	M.L. 1220.04	102-78	7.7	P.O. 124 1212.3	W bank
370	WEDGE H_2O	104-52	8.0	1212.0	HEADON
470		105-00	7.6	1212.4	"
470		102-00	6.9	1213.1	W bank
470		101-05	8.6	1211.4	CA / H_2O ±
470		100-20	6.8	1213.2	E bank
470		99-24	7.8	1212.2	Exposure
560		114-37	8.1	1211.9	Chan"

± 500' Bends(ch) west

Bends S 1/2" H_2O